





TECHNICAL REPORT HL-81-10

LOCK CULVERT VALVE LOSS COEFFICIENTS

Hydraulic Laboratory Investigation

Ьу

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September 1981 Final Report

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This report presents results of tests that were conducted to determine valve loss coefficients to use in predicting pressures downstream from navigation lock culvert valves. Reliable prediction of these pressures is needed so that a valve can be sited to prevent cavitation either by submergence or self-aeration with air vents. Tests were conducted with various culvert roof expansions beginning at several locations downstream from the lock culvert valve to determine the effect of the expansion on valve loss coefficients.

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PREFACE

The study reported herein was conducted under the sponsorship of the Office, Chief of Engineers (OCE), U. S. Army, as a Civil Works Investigation Work Unit 31479, in the Locks and Dam (Navigation Hydraulics) Research Program. The study was authorized in FY 77. Tests were conducted in the Hydraulics Laboratory of the U. S. Army Engineer Waterways Experiment Station (WES) under the general supervision of Messrs. H. B. Simmons, Chief of the Hydraulics Laboratory, and J. L. Grace, Jr., Chief of the Hydraulic Structures Division, and under the direct supervision of Mr. G. A. Pickering, Chief of the Locks and Conduits Branch. Tests were conducted by Messrs. D. B. Murray, J. H. Ables, Jr., J. F. George, C. L. Dent, T. E. Murphy, Jr., and H. S. Headley II. This report was prepared by Mr. Pickering.

Technical monitors of the Locks and Dams (Navigation Hydraulics)
Research Program during the course of the investigation and the preparation and publication of this report were Messrs. S. B. Powell and B.
McCartney (OCE).

Commanders and Directors of WES during the conduct of the study and the preparation and publication of this report were COL John L. Cannon, CE, COL Nelson P. Conover, CE, and COL Tilford C. Creel, CE. Techincal Director was Mr. F. R. Brown.

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CONVERSION FACTORS, U. S. CUSTOMARY TO METRIC (SI) UNITS OF MEASUREMENT

U. S. customary units of measurement used in this report can be converted to metric (SI) units as follows:

Multiply	Ву	To Obtain
cubic feet per second	0.02831685	cubic metres per second
feet	0.3048	metres
feet per second	0.3048	metres per second
feet per second per second	0.3048	metres per second per second

LOCK CULVERT VALVE LOSS COEFFICIENTS

Hydraulic Laboratory Investigation

PART I: INTRODUCTION

Background

- 1. Prevention of cavitation downstream from high-lift lock culvert valves has become an increasingly difficult problem for designers as lifts have increased to values greater than 100 ft.* High velocities and low pressures are induced as flow accelerates immediately downstream from the valves during the valve opening period. In some instances, the local flow acceleration is sufficient to lower the local pressure to the vapor pressure of water and form cavities within the flow. These cavities collapse rapidly or implode either in the water or against the downstream boundaries as they enter the increased pressure that results from the decreased velocity of flow as it expands and is decelerated in the culvert downstream of the valve. This has resulted in lock masters reporting loud pounding noises indicating cavitation implosions within the flow. In some instances, these booms have been violent enough to shake the lock walls and break windows. The implosion of the cavities against solid boundaries results in rapid pitting or damage to valves and appurtenances and to the concrete culverts.
- 2. In early designs, pressures low enough to cause cavitation were avoided by submerging the culvert at the location of the valve so that the pressure gradient was maintained above the top of the culvert. However, as lifts increased, it became increasingly costly to provide adequate submergence. Through prototype tests at some of the high-lift locks on the Columbia River it was found that admitting a controlled amount of air into the culverts at each valve virtually eliminated the

^{*} A table of factors for converting U. S. customary units of measurement to metric (SI) units is presented on page 3.

pounding noises. Air was drawn through a vent placed downstream from the valve into the culvert system during the valve opening period, was entrained as small bubbles in the highly turbulent flow, and emerged in the lock chamber so entrained that it merely caused the water to look milky. It was concluded that the air cushioned the collapse of the large cavities, eliminated shock pressures, and thus eliminated the pounding noises. This procedure allowed the culverts to be placed at a much higher elevation. Several locks have been constructed by the Corps using this procedure and no operation difficulties or hazardous conditions have been reported where pressures on the culvert roof were low enough to draw air during the valve opening period.

3. Through model tests of various locks it was found that expanding the culvert roof upward downstream from the valve would increase pressures on the roof of the culvert just downstream from the valve. Also, in one series of model tests for the Lower Granite Lock* it was found that the location of the expansion with respect to the valve directly affected the pressure on the roof of the culvert in the area immediately downstream from the valve as shown in Plate 1.

Purpose of Investigation

4. The use of expansions downstream from culvert valves is a very practical means of controlling the pressures and allowing the valves to be set at a more economical elevation. However, the limited amount of available test data was not adequate to predict the precise effect of the degree of expansion and location of the expansion on pressures and loss coefficients. Thus, systematic tests were needed to determine these factors. Also, it was expected that the tests would determine the exact location where minimum pressure occurs during a valve opening period.

^{*} U. S. Army Engineer Division, North Pacific, CE. 1979 (Sep). "Navigation Lock for Lower Granite Dam, Snake River, Washington; Hydraulic Model Investigation," Technical Report No. 126-1, Division Hydraulic Laboratory, Bonneville, Oreg.

PART II: TEST FACILITY

Description

5. The test facility (Figure 1) consisted of a headbay, conduit, valve well, reverse tainter valve, and tailbay. The upstream conduit was 47 ft long with a straight length of 17 ft upstream from the valve well and the downstream conduit was 14 ft long. A layout and details of the facility are shown in Plate 2. The culvert and valve well were constructed of plastic, and the valve was made from sheet metal.

Appurtenances

- 6. Water was supplied to the facility through a circulating system. Discharges were measured by a venturi meter and an orifice meter installed in the flow lines. Piezometers were used to measure pressures, and an adjustable tailgate was used to regulate the downstream pool elevation (lock chamber elevation).
- 7. The instrumentation and control system provided for operation of the culvert tainter valve by means of a programmable d-c motor. The position of the valve opening was indicated by a linear potentiometer. The cam and signal plot could be drawn to carefully control the valve position as a function of time.

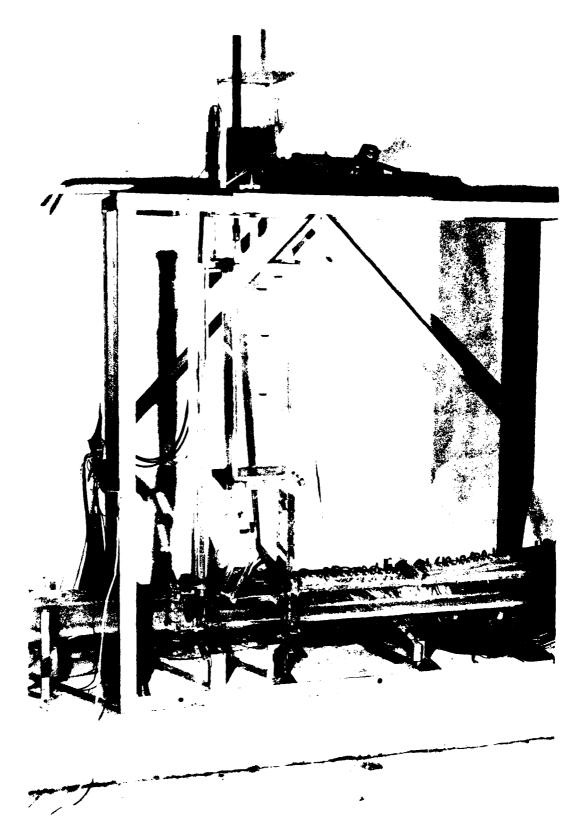


Figure 1. Test facility

PART III: TESTS AND RESULTS

8. Pressures downstream from lock filling valves are a function of the valve loss coefficients, $\rm K_{_{\rm V}}$, along with other factors. The valve loss coefficient used in this study refers to the total head loss at the valve which includes that due to the valve well, the valve, and the culvert expansion. This study was concerned primarily with the effect of culvert expansions downstream from the valve on $\rm K_{_{\rm V}}$. The valve loss coefficient is defined by the following equation.

$$K_{V} = \frac{\Delta E}{V_{1}^{2}/2g} \tag{1}$$

where

 K_{v} = valve loss coefficient

 ΔE = energy loss of the valve, ft

 ${\bf V}_1$ = average velocity in the culvert upstream from the valve, fps

g = acceleration due to gravity, ft/sec²

9. All of the tests reported herein were conducted with a vertically framed tainter gate as shown in Engineer Manual 1110-2-1610, "Hydraulic Design of Lock Culvert Valves." Although the valve loss coefficients reported herein would probably be slightly different with the other types of reverse tainter valves shown in the referenced manual, the conclusions drawn from these tests would be the same regardless of the type of valve used.

Test Procedure

10. Each test consisted of setting a specific valve opening, discharge, upper pool elevation, and lower pool elevation and then recording pressures as indicated by piezometers installed throughout the test section. At least three tests were made with each valve position with either different discharges or different lower pool (lock chamber) elevations. Data were plotted for each test as shown in Plate 3. Slopes of the pressure grade lines in the culverts upstream and downstream

from the valve section were extended to the valve well to determine the head loss, ΔH , at that section. Average velocities in the sections of culvert upstream and downstream from the roof expansion, V_1 and V_3 , respectively, were determined from the known cross-sectional areas and discharge. By adding the difference in velocity head in the two sections, $V_1^2/2g - V_3^2/2g$, to the head loss the total energy loss at the valve section, ΔE , was determined. The valve loss coefficient was then computed using Equation 1 shown in paragraph 8 above. Results for the various test runs along with pertinent boundary conditions for each run are shown in Table 1.

Initial Tests

- 11. Initial tests were conducted with a culvert of constant cross section 0.56 ft by 0.56 ft upstream, through, and downstream of the valve (type 1 design, Plate 4). Data obtained with this unexpanded culvert formed the basis for comparison with other designs tested and, also, for comparison with prototype data since extensive data were available from McNary Lock which has unexpanded culverts (Plate 5). Pressures measured with the type 1 design are shown in Table 2.
- 12. Data obtained were used to compute valve loss coefficients as indicated in paragraph 10. These coefficients are shown in Table 1 and are plotted in Plate 5. Points from the curve in Hydraulic Design Chart 534-1 are also shown for comparison. These data are very close and the agreement between the experimental and prototype values is excellent.
- 13. The assumption was made that energy loss between the valve well and the vena contracta is negligible. Thus, the velocity head in the vena contracta must equal the distance between the energy grade line in the valve well and the minimum pressure on the roof of the culvert downstream from the valve. On this assumption, velocities in the vena contracta and contraction coefficients for the valve were determined. Contraction coefficients agreed closely with those used in lock filling and emptying computations in Engineer Manual 1110-2-1610 as shown in Plate 6 for conditions of no culvert roof expansion. The expansions

tested in this study did not influence the contraction coefficient.

Culvert Expansion at Valve

14. After the base data were obtained, tests were conducted with culvert height expansions from 0.56 to 0.88 ft (type 2 design, Plate 4) and from 0.56 to 0.72 ft (type 4 design, Plate 4) beginning immediately downstream from the valve. The roof of the culvert was sloped up 1V on 10H in all designs. Pressures obtained during these tests are shown in Tables 3 and 4. Valve loss coefficients are shown in Table 1 and are plotted in Plate 7. As shown in this plot, there is greater energy loss through the expanded culverts, particularly in the 50 to 70 percent range of valve openings. With identical valve openings and equal discharge, pressure drops are the same regardless of the roof expansion, since the expansions did not influence the contraction coefficient. It is postulated that if the entire system (rather than the valve, as in these tests) controls flow, the pressure drops would be the same; but the absolute pressure downstream of the valve would be significantly higher. The test results indicate that the maximum negative pressure downstream from the valve is less with an expanded culvert, not because of flow circulation as had been hypothesized but because the fully expanded flow velocities (thus, discharges) are less in the downstream culvert, particularly through the range of valve openings that result in minimum pressure. With relatively small valve openings, the energy loss is relatively large due to expansion and deceleration of flow. With the larger valve openings, the change in velocities and energy loss are minor due to only minor contraction and expansion of flow.

Culvert Expansion Downstream from Valve

15. Tests were conducted to determine the effect of the position of the beginning of the roof expansion on valve loss coefficients. All of these tests were conducted with a roof expansion of IV on 10H from a height of 0.56 to 0.88 ft. Expansion started at distances downstream

from the valve of 0.28 ft (type 3 design), 0.56 ft (type 5 design), 1.68 ft (type 6 design), 2.24 ft (type 8 design), and 3.64 ft (type 7 design). All of these designs are shown in Plate 4.

16. Pressures measured during these tests are shown in Tables 5-9. Valve loss coefficients computed from these data and the data from the types 1 and 2 designs are shown in Table 1 and are plotted in Plate 8. These data show valve loss coefficients to be essentially the same with no roof expansion (type 1) and with roof expansions beginning 4.0 valve heights (type 8) and 6.5 valve heights (type 7) downstream from the valve. A plot showing the effect of the beginning of the roof expansion on valve loss coefficients is shown in Plate 9. It appears from this plot that the effect of the position of the roof expansion on valve loss coefficients varies slightly with the valve opening. For each valve opening there is a critical value for the distance to the beginning of the expansion, beyond which there is no change in the valve loss coefficient. Expansions that start downstream from these critical locations would have no influence on valve loss coefficients. This critical location is about 3.5 to 4.5 valve heights downstream of the valve in the range of openings where minimum pressure occurs during a filling cycle. This is in reasonable agreement with the Lower Granite results (Plate 1) which show effects within 5 valve heights.

Location of Minimum Pressure

17. Pressures were measured at various elevations and distances downstream from the valve to determine the location where minimum pressure occurs. These tests were conducted to assist the designer in locating the air vents downstream from the valve. The culvert expansions had little effect on the location of the minimum pressure. Isopiestic lines obtained with valve openings of 40, 50, 60, 70, and 80 percent are shown in Plate 10. These data are in dimensionless form and are averages from several tests conducted with the types 1 and 8 designs. The following was used to convert the data to a dimensionless form.

$$\frac{P_u - P}{v_1^2/2g}$$

where

 P_{ij} = pressure immediately upstream from valve well, ft

P = pressure at some point downstream from valve, ft

 V_1 = average velocity in culvert upstream from valve, fps

 $g = acceleration due to gravity, ft/sec^2$

These data indicate that minimum pressures occur near the top of the culvert. The distance downstream from the valve where these minimum pressures occur varies with the valve opening and moves upstream as the valve is opened. As shown in Plate 10, the location of minimum pressure at the roof of the culvert with the valve open 60 percent is between 0.5 and 1.0 valve heights downstream from the valve. Thus, the common practice of placing the air vents in the roof of the culvert about 0.5 valve heights downstream from the valve is satisfactory, although the vents could be placed farther downstream if necessary.

PART IV: DISCUSSION AND CONCLUSIONS

- 18. Accurate valve loss coefficients, particularly in the range of valve openings between 50 and 70 percent, are imperative for close prediction of minimum pressure downstream from navigation lock culvert valves. Reliable prediction of these pressures is needed so that a valve can be sited to prevent cavitation either by submergence or self-aeration with air vents. The valve loss coefficients determined in these tests unquestionably are more accurate than can be determined by picking values from filling curves only. Thus, it is recommended that in analysis of prototype data and in predictions of performance of future locks these coefficients be used.
- 19. The maximum negative pressure downstream from the valve was found to be less with an expanded culvert. The negative pressure was reduced because the valve loss coefficients were larger with the expanded culvert, and thus, the discharges were less through one range of valve openings that result in maximum negative pressure. The valve loss coefficients determined in this study can be used to determine the effect of culvert expansions on pressure downstream from the valve with expansions up to 57 percent of the valve height. The 57 percent expansion was based on the Lower Granite Lock which is the largest expansion constructed to date. Also, this was considered to be near the upper limit from a practical standpoint.
- 20. The study showed that culvert expansions that begin 4.5 valve heights or more downstream from the valve have no effect on the valve loss coefficients for valve openings of 30 percent or greater. Expansions beginning within 4.5 valve heights of the valve increased loss coefficients linearly as the expansion was placed closer to the valve. This agrees reasonably well with data obtained from a previous model of Lower Granite Lock which shows minimum pressure decreasing linearly as the expansion was moved downstream until it reached a distance of 5 valve heights.
- 21. In design of future locks if it becomes necessary to expand the culverts to reduce friction losses in the filling system or for

structural reasons, and the expansion is not needed to reduce negative pressures for optimum location of the valve, then the expansion should not begin within 4.5 valve neights downstream from the valve. If the expansion is needed to reduce negative pressures, but the amount of expansion is greater than that required to obtain optimum pressures with the expansion beginning immediately downstream from the valve, the expansion can be moved some distance downstream from the valve to obtain optimum pressures. The valve loss coefficients shown in this report can be used to determine this distance.

- 22. It was concluded that the contraction coefficient is independent of culvert roof expansions when the valve is controlling the discharge as it was in these tests. The pressure drop from the grade line in the valve well to the minimum pressure downstream from the valve was dependent upon both the contraction coefficient and the discharge. Thus, expansions influenced this pressure drop only because they influenced the discharge.
- 23. Minimum pressure downstream from the valve occurred at or near the top of the culvert. The location of this pressure varied with the valve opening and moved upstream as the valve was opened. The minimum pressure was located between 1.0 to 0.5 valve heights downstream from the valve with valve openings in the range of 50 to 70 percent open where minimum pressure usually occurs. Thus, air vents should be located in the roof of the culvert at a distance of 1.0 to 0.5 culvert heights downstream from the valve, preferably 0.5 culvert heights, since the lowest pressure occurs at that location with the valve near a 60 percent opening.
- 24. All of the data shown in this report were obtained with a vertically framed (Holt-type) valve, since it is the most commonly used type. Valve loss coefficients and contraction likely are different for other types of valves, such as a double skin-plate valve. Although the value of the coefficients would be different, the conclusions concerning the effect of expansion and location of the expansion on loss coefficients and location of minimum pressure should be the same.
 - 25. The test facility used to obtain data to determine the valve

loss coefficients did not include the culvert intake or distribution culverts and ports of the filling and emptying system. Also, the tests were conducted with constant upper and lower pool elevations and valve openings. Thus, the effective inertia of a prototype filling and emptying system was not reproduced. However, by using the valve loss coefficients determined in this study, along with other loss coefficients for the culvert intakes, friction, and exit manifold in the CORPS* H5320 computer program, accurate hydraulic data such as pressures and lock filling and emptying times can be obtained.

26. Future studies with a model of an entire bottom longitudinal filling and emptying system would be very beneficial in determining other loss coefficients such as the intakes to the culverts, in the distribution system and at the outlet manifolds.

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^{*} Conversationally Oriented Real-Time Program Generating System (CORPS) Computer Program H5320, "Lock Filling and Emptying Symmetrical Systems." Available from: WES Library, U. S. Army Engineer Waterways Experiment Station, CE, P. O. Box 631, Vicksburg, Miss. 39180, and from several CE computer systems.

Table 1

Valve Loss Coefficients and Hydraulle Conditions

Land		1				Valva	Type	-			:		7.0102	12.5	1	1		:	1	Value
Culver					Dis-	Loss	Culvert	Valve			Lock	-410	Lobs	Culvert	Valve			Lock	515-	Luss
Expan- sion	Opening	Run No.	Headwater Elevation	Chamber Elevation	charge CFS	Coef- fictent	Expan-	Opening Percent	Run No.	Headwater Elevation	Chamber Elevation	charge CFS	Coet- ficient	Expan-	Opening Percent	Kur S	Headwater Elevation	Chamber Elevation	charge CFS	Coef- factent
-	0,7	3.53	5.750		0.60	56.14	^	07	1 5	3.972	1.200	. 17		-	9	270	086.	. 308.1	1.00	0.197
	70	3	5.230	1.870	0.60	55.79		0,	716	4.572	1.828	===	11.39		100	271	5.360	7.440	3	0.081
	2	334	4.710	1.190	09.0	58.42		0,7	217	5.172	2.400	Ξ:	10.99		100	272	0880	1.800	<u> </u>	7.00.0
	e.	30.	7987	1.232	8 8	20.25		0, 0,	2 18	5.75.	2.412	1.58	26.01	٠	9 %	27.2	2.200 2.200	7.000	7. Fe 1. GE	50.08
		207	5.852	2,248	00.1	19.68		<u> </u>	220	2.400	1.816	 x	. 39		Ş	275	5.570	1.800	1.983	10.17
		197	5.804	1.200	7.	19.51		20	221	4.660	1.200	. 58	1.4.		€ ;	177	3.970	1.400	0.8°	22.48
	3	661	5.312	1.240	1.08	20.00		09	223	5.872	2.420	2. to	6.63		<u> </u>	20 0	000	00		96.01
	9	196	3.672	1.200	5.1	9.16		9 9	22.5	5.216	1.828	2.10	26.5			280	068.7	2.400	1.13	9.85
		195	4.920	2,384	1.13	9.26		20,	227	5.888	2,400	æ,	1.52			 	5.000	1.246	1.36	10.00
		155	5.608	1.160	1.54	8.90		70	228	5.348	1.840	2.48	1.5.1			383	4.310	1.200		10.25
		2.5	4.212	1.204	1.27	8.55		2 5	229	4.872	1,240	2.48	1.56		ξ		4.635	1.100	 	5.27
	ο <u>ς</u>	17.5	4.440	1.136	68	4.30		S &	231	5.428	2,448	19.7	2.50			6 8	5.070	2,400	C 40	5.05
		177	5.552	2.436	. 68	70.7		80	232	4.248	1,208	2.61	0.60			787	5.115	1.200	1.85	98.
		157	3.928	1,324	1.54	4.01		06	233	5.396	2.396	2.87	0.27		90	887	1.180	1.200	110	2.51
		184	4.388	1.208	1.65	4.43		06	234	4.828	1,788	2,82	1			687	5.100	1.890	. 10	17.73
	90	167	5.016	1.200	2.08	2.08		100	235	5.408	2.408	2.93	0.11			267	5.550	2.400	٠. اد اد	7
		168	5.108	1.800	2.08	1.92		100	236	4.820	1.812	7.93	0.13				2000	20 20	2 3	6
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		159	5.584	1.312	2.35	2.06			244	4.565	1,885	1.13	1.74			367	5.140	1.200	2.60	J. 50
	70	172	5.800	2.152	2.48	0.94			245	5,080	7.400	1.13	1.73			5	650	1.200	æ: €:	1.33
		171	5.420	1.800	2.48	0.91			246	5.190	1.200	1, 38	1.75		æ	367	425	1.190	<u>ء</u> :	0.60
		178	5.380	1.600	2.48	00.0			247	4.465	1.200	1.23	1.83			5 G	4.435	1.820	e : .	<u> </u>
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		- 61	5.580	967 -	2.00	0.45			250	5.670	2 400	1.68	62.5		O P	9	5.430	2.400	2	0.23
	80	320	4.730	1.220	19.7	0.344			251	5,165	2.410	8.	5.58		06	104	5,020	1.800	.8	J 36
		321	5, 190	1.810	2.61	0.409			252	5.205	1.200	1.85	5.22		5	303	5.390	1.800	3.00	0.213
		322	5.770	7.440	2.61	0.307		9	253	4.605	1,200	2.10	2.76		100		5.550	5.400	<u>.</u>	\$50.0
		323	4.910	1.300	2.72	0.368			254	5,310	1.805	2.10	2.70		001	<u> </u>	5.150 2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.	1.800	- a	0.000
	9	\$ 2	5.830	057.	80.0	0.097			25.5	5.520	1 200	: : : :	2.75	ŗ	9.5	335	5.720	500	0	50.19
	?	356	0.430	1,410	2.80	0.097			257	5.875	1.200	2.48	2.69		50	3.55	5.460	1.820	0.60	60.00
		327	4.820	1.170	2.80	0.097		70	258	4.645	1.206	7.48	1.37		0,	337	6.8.5	1.320	0.60	9.72
		328	5.860	1.180	3.00	0.106			259	5.205	1.800	87.7	3.		Œ	98 5	3.680	1.190	0.80	se Se
	001	329	5.770	2,416	2.76	0.042			260	5.435	2.390	2,48	87.			5 2 2	2.330	1.800	0.30	φ ç
	5 5	9.5	5.220	1.770	7.76	0.050			2,41	4.950	1.700	04.7				7	350.4	9 9	6 - 6 -	· · ·
	Ē	200	7.760		£ 6	1, 04,		ă	207	2.400	1 200	1.00	76.0		Q.	; ;	3.430	1.180	- 1	: 3
	2	200	2 776	1.808	08.0	200			797	0.9.7	1.820	2.61			9	2	4.470	1.820	= = =	10.69
		210	4.872	077	0.80	21.98			265	5.230	2.410	2.61	0.62		9	344	5,160	2.400	1.13	10.79
		211	4.804	1,220	0.96	21.51			266	4.360	1,200	2.72	0.62		C,7	345	5.090	1.220	1.38	10.53
		212	5.104	1.212	1.00	22.41			767	5.560	1.200	3.18	79.0		0,5	9.7	4,510	1.200	φ. 	5: 53
		213	5.580	1,300	 	5. 5. 5.		G 8	268	5.250	2,380	٠. د چې و	0.247			2 Z	5. 140 5. 640	1.850	£ 4	, , ,
		517	3.480	7(8.1	5.	(12.13		ĵ.	5 E 3	4.1/0		ć .	16.5			į		200	3011	: :
										(Cont Inved.)	ed)									

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Valve	loss	Coef-	ficient	0.248	0.226	0.218	0.166	0.170	0.150	22.8	19.6	16.7	9.58	9.66	2.45	4.12	4.31	4.19	3.98	2.87	2.91	2.81	2.55	30.	1.92	96.	66.1	1.99	1.97	1.42	1.53	1.35	1.29	0.32	78.0	1.06	0.4.	0.37	0.36	
	Dis-	charge	CFS	3.90	2.70	3.00	2.76	2.93	3.18	0.75	0.90	1.10	06.0	1.20	1.50	1.40	1.60	1.84	2.00	1.70	1.90	2.10	2.30	1.80	00	0, 50	, C. c	2.10	1.92	1.90	2.20	7.50	2.68	5.00	2.52	80	07.7	2.80	1, 10	
	Lock	Chamber	Elevation	1.970	1.810	2.300	2.100	2.310	1.940	1.110	1.620	1.680	1.120	1.090	1.620	1.300	1.230	1.760	1.740	1.020	1.270	1.610	1.860	1.160	1.390	1.520	000	1.130	1.090	1.040	1.180	7.200	2.120	0.96.0	1.600	080	1.710	0.0.	ુ: 33હ	
		Headwater	Elevation	5.180	7.490	5.510	4.755	5.245	5.460	3.330	4.450	5.220	2.670	3.790	5.180	3,290	3.840	5.140	5,520	3.350	4.170	5.070	5.670	3, 380	3.920	5.210	5 100	3.980	3.455	3.183	4.250	5.630	5.890	3.020	4.720	5.870	3.7.	5,230	5.840	
		Run	No.	907	407	807	403	707	405	433	434	435	36	437	96.7	68.5	0,7	155	777	£ 1,1	177	445	91.7	1.7	00 :	7	007	. 63	9,	151	3	453	75.7	455	156	121	χ,	757	Ę,	
	Valve	Opening	Percent	06	90	96	100	100	100	30	30	30	04	07	0,7	20				55				09						65				7.0	20	7.0	90	80	ž	:
Туре	Culvert	Expan-	ston	7						œ																														
Valve	Loss	Coef-	ficient	1.48	1.49	1.51	1.04	1.02	1.03	0.483	0.464	0.460	0.239	0.218	0.226	0.133	0.113	0.141	19.87	19.61	19.80	8.67	8.76	9.36	3.89	3.86	9 5	2.67	2.56	96.1	1.98	7	1.44	1.4.1	77.1	1.01	66.0	1.01	0.465	1000
	Dis-	harge	CFS	2.60	2.40	2.20	2.48	2.80	2.15	2.61	3.00	2.80	2.85	3.00	2.70	2.93	3.18	2.76	1.00	0.90	0.80	1.38	1.13	0.89	85	£ .	300	00	1.80	87.7	3.10	1.92	7.60	2.40	2.20	7.80	87.	3.15	7.61	2 80
			Elevation																																					
		Headwater	Elevation	5.630	4.825	4.030	4.740	9.460	4.060	4,385	5.330	4.965	4.810	5.410	4.910	5.190	5.580	4.580	5.285	4.550	4.010	5.010	3.710	5.690	4.970	7.70	5.420	4.780	1.935	5.545	4.630	3.920	5.520	4.535	3.975	5.430	096.7	4,310	087.7	5 280
		Run	c.	700	401	402	385	386	387	388	389	390	391	392	393	394	395	396	430	431	:35	427	428	459	424	??	429	422	423	418	617	420	517	416	417	412	413	717	605	019
	Valve	Opening	Percent																								S 52													
Type	Culvert	Expan-	ston	9															7																					
valve	Loss	Coef-	ficient	5.35	5.17	2.54	2.61	2.59	2.49	2.48	1.24	1.27	1.24	1.26	1.25	0.539	0.576	!	0.591	0.576	0.223	0.215	0.211	0.118	680.0	21.00	20.10	19.37	21.09	10.10	6.47	9.36	4.51	4.83	4.33	2.96	3.02	2.91	2.11	2.13
;	Dis-	charge	CFS	1.48	1.85	2.10	2.10	2.10	2.35	2.48	2.48	2,48	2.48	2.60	2.80	2,61	2.61	2.61	2.72	3.18	2.82	2.82	9.00	2.93	2.93	2 6	0.80	1.00	0.0	1.13	7.38	0.89	1.68	1.48	1.85	2.20	2.00	1.80	2.10	2.48
	Lock	Chamber	Elevation	1.210	1.220	1.190	1.830	2.440	1.260	1.170	1.190	1.775	2.400	1.220	1.190	1.200	1.800	2.440	1.150	1.230	2.430	1.790	1.800	2.400	1.870	1.000	1.720	1.830	1.830	1.690	1.800	1.265	1.790	1.170	1.700	1.810	1.675	1.470	1.780	1.410
		Headwater	Elevation	3.860	5.170	4.370	5.090	5.620	5.210	5.470	4.280	4.930	5.580	4.710	5.200	3.930	4.520	5.130	4.220	5.350	5.200	4.620	4.930	0/7.6	4.710	610	3.980	5.240	4.840	4.230	5.340	2.730	4.725	3.600	5.130	5.580	4.900	4.040	4.720	5.380
		Run	9	349	320	351	352	323	354	355	326	357	358	359	360	361	362	363	364	365	366	367	268	203	3/0	37.	373	374	375	376	377	378	379	380	8	397	398	366	382	383
	Valve	Opening	Percent			09					0/				4	80				;	3 3	S (2 G	3 5	3 5	8 9	•			07	0,4	40	20	9,	20	22	55	55	09	09
		,	ston	~																						æ	,													

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(Sheet 1 of 3)

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Average Piezometer Readings, Type 1 Expansion

Pie	Piezometer Locations	ocations							Run	n Number*	*						
2	Station	Elevation	332	333	334	198	201	202	197	199	194	196	195	155	156	175	176
4	15.00U	0.56	5.62	5.11	4.58	4.53	5.12	5.50	5.36	5.10	3.23	3.89	4.47	4.83	3.68	3.52	4.06
S	8.79U	_	5.61	5.10	4.57	4.49	5.08	5.47	5.31	5.06	3.16	3.83	4.42	4.74	3.62	3.40	3.96
9	6.75U		5.60	5.09	4.56	4.48	2.07	2.46	5.30	5.04	3.15	3.82	4.40	4.72	3.61	3.39	3.94
7	4.79U		5.60	5.09	4.56	4.48	5.06	5.45	5.29	5.03	3.14	3.81	04.4	4.70	3.59	3.36	3.91
∞	2.79U		5.60	5.09	4.55	4.47	5.05	5.44	5.28	5.02	3.13	3.80	4.39	69.7	3.59	3,35	3.91
6	1.790		5.59	5.08	4.55	95.4	5.03	5.43	5.27	2.00	3.12	3.79	4.38	7.66	3.57	3.31	3.85
14	0.080		1.61	1.12	0.40	0.08	0.57	1.06	-0.32	-0.18	0.14	0.80	1.38	-0.68	0.00	-0.22	0.42
15	0.22D		1.60	1.11	0.39	ł	;	!	}	}	}	;	ł	;	;	!	;
16	0.36D		1.59	1.10	0.38	90.0	0.56	1.04	-0.34	-0.20	0.12	0.78	1.35	-0.70	-0.02	-0.30	0.42
17	0.50D		1.58	1.09	0.37	90.0	0.52	1.03	-0.36	-0.22	0.10	0.76	1.33	-0.74	-0.04	-0.32	0.40
18	0.64D		1.57	1.08	0.37	0.05	0.51	1.02	-0.36	-0.23	0.09	0.76	1.32	-0.76	-0.06	-0.30	0.44
19	0.78D		1.58	1.08	0.37	0.04	0.52	1.01	-0.36	-0.24	0.08	0.75	1.32	-0.79	-0.06	-0.26	0.44
20	0.92D		1.59	1.09	0.38	0.04	0.54	1.02	-0.36	-0.26	0.10	0.77	1.34	-0.78	-0.06	-0.24	97.0
21	1.06D	-	1,61	1.10	0.39	0.05	0.56	1.04	-0.34	-0.22	0.14	0.84	1.36	-0.74	-0.04	-0.22	0.50
22	1.20D		1.63	1.12	0.40	0.07	0.63	1.07	-0.30	-0.20	0.16	0.86	1.38	-0.68	0.04	-0.12	0.60
23	1.34D	-	1,65	1.13	0.43	0.09	0.65	1.10	-0.28	-0.12	0.20	0.88	1.42	-0.64	0.10	0.04	0.68
54	1.48D		1.68	1.16	97.0	0.16	0.68	1.16	-0.22	-0.10	0.28	0.94	1.44	-0.60	0.20	0.10	98.0
25	1.62D		1.71	1.19	0.50	0.25	0.73	1.21	-0.16	0.04	0.32	1.00	1.50	-0.46	0.24	0.30	0.92
56	1.76D		1.75	1.24	0.54	0.28	0.76	1.34	-0.08	0.10	0.36	1.10	1.60	-0.36	0.32	0.40	1.00
27	1.90D	-	1.78	1.30	0.58	0.34	0.84	1.40	-0.02	0.18	0.48	1.16	1.64	-0.24	07.0	0.50	1.10
28	2.04D	-	1.87	1.36	0.65	0.44	96.0	1.48	0.08	0.24	0.54	1.24	1.76	0.00	97.0	0.74	1.30
59	2.18D		1.93	1.42	0.74	0.50	1.06	1.66	0.22	97.0	0.64	1.44	1.82	0.12	09.0	0.92	1.40
30	2.46D		2.10	1.58	0.92	0.80	1.24	1.80	65.0	0.70	0.84	1.56	5.04	77.0	0.74	1.00	1.60
31	2.74D		2.20	1.74	1.07	0.88	1.46	1.96	0.76	0.88	1.00	1.68	2.24	0.76	0.96	1.12	1.88
32	3.02D		2.30	1.82	1.15	1.06	1.66	2.16	96.0	1.10	1.08	1.72	2.40	96.0	1.06	1.26	1.92
33	3.30D		2.34	1.86	1.18	1.16	1.76	2.24	1.08	1.20	1.16	1.80	2.46	1.04	1.16	1.30	1.94
34	3.58D		2.37	1,88	1.19	1.30	1.80	2.28	1.20	1.27	1.20	1.88	2.47	1.20	1.24	1.32	1.96
35	3.86D		2.38	1.89	1.20	1.30	1.82	2.29	1.24	1.29	1.22	1.90	2.48	1.24	1.27	1.34	1.98
36	4.80D		2.38	1.89	1.20	1.31	1.83	2.30	1.27	1.30	1.22	1.90	2.48	1.28	1.29	1.34	1.98
37	007·9		2.38	1.89	1.20	1.32	1.84	2.31	1.28	1,30	1.24	1.91	2.49	1.28	1.29	1.34	1.98
39	9.60D		2.38	1.89	1.20	1.30	1.82	2.28	1.24	1.27	1.20	1.88	2.45	1.23	1.26	1.28	1.91
70	11.15D	-	2.37	1.88	1.19	1.28	1.81	2.27	1.24	1.26	1.20	1.86	2.44	1.22	1.25	1.26	1.88
41	12.70D	_	2.37	1.88	1.19	1.29	1.80	2.27	1.23	1.24	1.18	1.8.	2.44	1.21	1.24	1.24	1.88
								(Continued)	(pən								

* Refer to Table 1 for flow conditions for each run.

Table 2 (Continued)

	170	2.93	2.73	2.68	2.60	2.62	2.52	-0.20	;	-0.24	-0.20	-0.12	0.04	0.28	0.56	0.68	0.84	0.92	1.08	1.20	1.26	1.30	1.32	1.42	1.46	1.48	1.48	1.50	1.50	1.48	1.48	1.33	1.28	1.26
	178	3,36	3.14	3.10	3.07	3.04	2.98	0.15	1	0.18	0.20	0.26	0.42	99.0	0.80	1.06	1.16	1.32	1.48	1.60	1.66	1.68	1.72	1.74	1.76	1.80	1.82	1.86	1.88	1.88	1.86	1.73	1.69	1.66
	171	3.48	3.26	3.22	3.16	3.16	3.09	0.36	;	0.40	97.0	0.50	09.0	0.76	1.04	1.32	1.40	1.60	1.64	1.72	1.84	1.88	1.94	1.96	2.00	5.04	5.06	2.08	2.08	5.06	2.06	1.91	1.38	1.86
	172	3.82	3.63	3.58	3.55	3.53	3.44	0.74	}	0.76	0.80	0.86	1.06	1.28	1.36	1.56	1.72	1.88	1.94	2.08	2.14	2.20	2.26	2.28	2.30	2.36	2.38	2.40	2.42	2.45	7.40	2.26	2.23	2.21
	159	3.78	3.60	3.56	3.53	3.50	3.43	-0.68	;	-0.72	-0.76	-0.76	-0.72	-0.80	-0.44	-0.20	0.02	0.24	0.42	0.60	0.74	0.84	1.04	1.24	1.37	1.45	1.48	1.53	1.56	1.54	1.52	1.38	1.36	1.33
	163	3.74	3.56	3.52	3.48	3.46	3.40	-0.55	ì	-0.56	-0.57	-0.55	-0.48	-0.40	-0.26	-0.04	0.16	0.38	0.58	0.76	0.92	1.07	1.18	1.30	1.36	1.44	1.50	1.53	1.55	1.57	1.56	1.44	1.42	1.40
100	179							-			-	-																						
un Numbe	174	3.49	3.34	3.30	3.28	3,27	3.21	-0.06	}	-0.08	-0.10	-0.06	0.00	90.0	0.16	0.32	0.72	0.88	96.0	1.08	1.14	1.20	1.36	1.44	1.50	1.58	1.64	1.68	1.70	1.69	1.68	1.56	1.55	1.49
	169																																	
	168	3.76	3.61	3.59	3.56	3.54	3.49	0.40	1	0.36	0.38	9.70	94.0	0.52	0.56	0.84	1.06	1.20	1.32	1.48	1.60	1.68	1.72	1.88	1.92	5.00	5.06	2.08	2.08	5.06	5.06	1.95	1.93	1.92
	167	3.18	3.02	2.98	2.96	2.95	2.90	-0.40	1	-0.44	-0.48	-0.36	-0.36	-0.28	-0.20	0.08	0.20	0.28	0.72	0.80	0.84	0.88	1.08	1.16	1.24	1.28	1.36	1.38	1.37	1.36	1.37	1.25	1.24	1.21
	184	3.47	3,35	3.34	3.32	3.30	3.28	-0.24	;	-0.28	-0.29	-0.27	-0.24	-0.21	-0.19	-0.12	-0.02	0.10	0.28	0.40	0.51	0.64	0.82	1.00	1.12	1.25	1.32	1.34	1.36	1.36	1.35	1.27	1.26	1.25
	157	3.18	3.10	3.08	3.06	3.06	3.02	0.14	!	0.12	0.11	0.10	0.11	0.12	0.20	0.30	0.40	0.52	09.0	0.72	0.82	0.84	1.04	1.10	1.28	1.34	1.38	1.42	1.42	1.43	1.43	1.38	1.37	1.36
	177	4.70	7.60	4.58	4.55	4.54	4.51	1.10	1	1.08	1.04	1.08	1.12	1.14	1.16	1.28	1.32	1.48	1.52	1.64	1.96	2.08	2.14	2.32	2.40	2.52	2.56	2.62	2.65	2.64	2.58	2.58	2.56	2.56
cations	Elevat ion	0.56								_		-									_			-	_									-
Piezometer Locations	Station	15.000	8.790	6.750	4.790	2.79U	1.790	0.080	0.22D	0.360	0.50D	0.640	0.780	0.92D	1.06D	1.20D	1.34D	1.485	1.62D	1.76D	1.90D	2.04D	2.18D	2.46D	2.74D	3.02D	3.30D	3.58D	3.860	4.80D	6.40D	009.6	11.150	12.70D
Piez	No.	4	5	9	1	ၹ	6	14	15	16	17	18	19	20	21	22	23	54	25	56	27	87	56	30	31	32	33	34	35	36	37	39	04	41

Table 2 (Concluded)

	331	2.92	2.63	2.53	2.52	5.49	2.37	2.23	2.25	2.25	2.26	2.26	2.27	2.27	2.26	2.26	2.25	2.25	2.24	2.23	2.23	2.22	2.21	2.21	2.21	2.18	2.16	2.17	2.17	2.15	2.10	1.99	1.85	1.90
	330	2.73	2.48	2.39	2.38	2.36	2.26	2.13	2.14	2.14	2.15	2.15	2.16	2.16	2.15	2.15	2.14	2.14	2.13	2.13	2.13	2.13	2.12	2.12	2.13	2.10	2.08	5.09	5.09	7.06	2.02	1.93	1.80	1.85
	329	3.33	3.10	3.01	3.00	2.98	2.87	2.75	2.76	2.77	2.78	2.79	2.80	2.80	2.79	2.79	2.78	2.78	2.77	2.77	2.77	2.76	2.75	2.75	2.75	2.72	5.69	2.70	2.70	2.67	2.63	2.55	2.45	5.49
	328	3.00	2.74	2.63	2.62	7.60	2.46	1.45	1.73	1.95	2.11	2.17	2.20	2.21	2.21	2.21	2.21	2.21	2.21	2.21	2.21	2.21	2.20	2.20	2.21	2.17	2.13	2.15	2.16	2.13	5.09	1.99	1.83	1.90
	327	2.26	7.00	1.90	1.88	1.86	1.74	0.84	1.12	1.33	1.45	1.51	1.53	1.54	1.54	1.54	1.53	1.53	1.52	1.51	1.51	1.51	1.50	1.50	1.50	1.47	1.45	1.47	1.48	1.46	1.42	1.32	1.17	1.23
	326	2.91	2.67	2.59	2.55	2.53	2.43	1.51	1.74	2.00	2.12	2.18	2.20	2.21	2.21	2.21	2.20	2.20	2.20	2.19	2.19	2.18	2.17	2.17	2.17	2.15	2.13	2.14	2.14	2.12	5.09	2.00	1.85	1.91
	325								2.28	•																							2.30	
Run Number	324	2.78	2.52	2.40	2.38	2.36	2.24	0.18	0.16	0.30	0.48	0.73	0.99	1.20	1.38	1.45	1.51	1.54	1.55	1.56	1.58	1.58	1.59	1.59	1.60	1.59	1.58	1.59	1.60	1.57	1.54	1.43	1.27	1.33
R	323																																	
	322	3.61	3.38	3.33	3.29	3.26	3.17	1.66	1.65	1.70	1.85	2.06	2.27	2.44	2.55	2.58	2.61	2.65	2.67	2.68	2.69	5.69	2.70	2.71	2.71	2.70	2.70	2.70	2.70	2.69	2.67	2.59	5.49	2.52
	321	3.00	2.79	2.73	5.69	2.66	2.60	1.03	1.02	1.06	1.23	1.40	1.59	1.76	1.91	1.99	2.03	2.02	2.07	2.08	5.09	2.10	2.11	2.12	2.12	2.12	2.10	2.10	5.09	2.07	5.04	1.96	1.86	1.89
	320	2.48	2.26	2.21	2.15	2.13	2.04	0.43	0.39	0.43	99.0	0.83	1.03	1.15	1.28	1.40	1.44	1.48	1.51	1.52	1.53	1.54	1.55	1.56	1.57	1.56	1.55	1.54	1.54	1.50	1.48	1.40	1.29	1.32
	160	2.76	2.54	2.56	2.51	2.48	2.42	-0.08	}	-0.06	-0.04	0.04	0.12	0.28	0.32	0.72	0.92	1.12	1.08	1.16	1.24	1.28	1.32	1.40	1.44	1.46	1.46	1.48	1.47	1.47	1.46	1.33	1.30	1.28
	191	3.23	2.99	2.94	2.90	2.86	2.78	-0.42	!	-0.46	-0.50	-0.24	-0.12	0.08	0.28	0.52	0.68	0.92	1.04	1.16	1.26	1.32	1.42	1.50	1.53	1.57	1.53	1.54	1.58	1.56	1.54	1.40	1.36	1.34
cations	Elevation	0.56		_							_										_				_		-			_		_	-	>
Piezometer Locations	Station	15.000	8.79U	6.75U	4.79U	2.790	1.79U	0.080	0.22D	0.36D	0.500	0.640	0.78D	0.92D	1.06D	1.20D	1.34D	1.48D	1.62D	1.760	1.90D	2.04D	2.18D	2.46D	2.74D	3.02D	3.300	3.58D	3.86D	4.40D	6.40D	9.60D	11.15D	12.70D
Pie	Š	4	5	9	7	æ	6	14	15	16	13	18	19	50	21	22	23	54	25	97	27	28	53	30	31	32	33	34	35	36	37	39	0,4	41

Table 3

Average Piezometer Readings, Type 2 Expansion

Plezomer , ocations				Run Numb	er*					
209 2		211 212	2 213	214	215	216	217	218	219	220
				5.36	3.51	4.17	4.74	4.52	4.85	77.7
				5.31	3.46	4.10	4.68	77.7	4.75	4.32
				5.30	3.45	4.09	4.66	4.45	4.74	4.30
				5.30	3.44	4.08	4.66	4.4]	4.72	4.28
_				5.29	3.42	4.08	4.65	4.40	4.70	4.27
_				5.28	3.40	4.07	4.62	4.38	7.66	4.24
				1.18	0.38	1.09	1.74	0.00	1.40	0.70
				1	1	-	1	1	!	1
_			_	1.18	0.40	1.09	1.73	-0.01	1.38	69.0
_			_	1.18	0.40	1.08	1.73	-0.03	1.36	0.68
	0		_	1.18	0.38	1.07	1.72	0.00	1.37	0.67
				1.18	0.38	1.06	1.71	0.00	1.38	99.0
			_	1.18	0.39	1.08	1.70	0.02	1.42	0.69
_			_	1.18	0.39	1.09	1.71	0.05	1.44	0.74
_				1.18	0.40	1.09	1.74	(.03	1.48	0.75
			_	1.18	0.44	1.10	1.76	90.0	1.52	0.80
	0		_	1.20	0.44	1.11	1.79	0.08	1.56	0.82
1.28 1.90	0		_	1.20	97.0	1.12	1.79	0.08	1.62	0.88
_	ن		_	1.22	0.47	1.12	1.80	0.12	1.66	96.0
_	0		_	1.22	0.56	1.16	1.82	0.16	1.70	1.00
	0		_	1.26	0.58	1.18	1.86	0.18	1.74	1.04
			_	1.28	0.58	1.21	1.88	0.21	1.82	1.08
			_	1.28	09.0	1.23	1.90	0.28	1.94	1.24
			_	1.34	0.64	1.28	1.98	0.34	2.00	1.30
_			_	1.37	0.70	1.36	2.01	0,40	2.14	1.40
			_	1.50	0.74	1.44	2.06	74.0	2.20	1.41
			_	1.51	0.80	1.52	2.12	0.60	2.26	1.60
	0		_	1.56	1.00	1.60	2.26	0.72	2.36	1.64
				1.62	1.21	1.80	2.40	1.12	2.58	1.70
				1.92	1.21	1.87	2.52	1.21	2.60	2.00
				2.00	1.22	1.86	2.51	1.19	2.58	1.99
				2.00	1.21	1.86	2.50	1.19	2.56	1.98
				2 00	נכו	1 0.4	000	9.	2,4	00

* Refer to Table 1 for flow conditions for each run.

Table 3 (Concluded)

Startion Elevation Color Color	Piezometer Locations	cations						Ru	n Number						
0.56 4,43 3.80 3.30 3.88 3.31 2.76 3.14 2.56 1.93 2.73 2.12 1.42 4.24 3.60 3.69 3.54 3.00 2.46 2.83 2.23 1.66 2.43 1.65 2.44 1.75 4.18 3.45 3.60 3.54 2.98 2.42 2.79 2.17 1.57 2.13 1.75 4.18 3.55 3.05 3.43 2.87 2.90 2.46 2.83 2.13 1.52 2.25 1.55 2.13 1.75 2.13 1.75 2.13 1.75 2.13 1.75 2.13 1.75 2.13 1.75 2.13 1.75 2.13 1.75 2.14 1.3 3.48 2.29 3.43 2.87 2.30 2.66 2.03 1.52 2.20 1.55 2.00 1.55 2.00 2.60 0.90 0.35 -0.34 0.80 0.19 -0.46 1.11 0.38 -0.11 1.21 0.58 1.25 0.05 0.05 0.03 0.03 -0.38 0.75 0.17 0.04 0.10 0.04 0.08 0.13 -0.38 0.75 0.17 0.04 0.10 0.46 0.02 0.13 0.14 0.15 0.14 0.15 0.14 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15	ion	Elevation	223	224	226	227	228	229	230	231	232	233	234	235	236
4.27 3.63 3.11 3.64 3.06 2.50 2.88 2.28 1.66 2.43 1.81 1.81 4.22 3.60 3.59 3.48 2.95 2.40 2.73 2.13 1.65 2.43 1.75 4.18 3.45 3.05 3.48 2.95 2.40 2.73 2.13 1.57 2.31 1.70 2.41 3.48 2.95 2.40 2.75 2.13 1.57 2.31 1.70 2.60 0.57 0.94 0.36 -0.34 0.80 0.19 -0.46 1.11 0.38 -0.11 1.21 0.58 0.60 0.50 0.50 0.35 -0.35 0.76 0.19 -0.46 1.11 0.38 -0.11 1.21 0.58 0.60 0.50 0.33 -0.34 0.38 0.19 -0.46 1.11 0.38 -0.11 1.21 0.58 0.60 0.50 0.39 0.34 -0.38 0.75 0.17 -0.46 1.12 0.48 0.04 0.05 0.05 0.05 0.05 0.05 0.05 0.05	200	0.56	4.43	3.80	3,30	3.88	3.31	2.76	3.14	2.56	1.93	2.73	2.12	2.51	1.91
4,24 3,56 3.69 3.58 3.02 2.46 2.83 2.23 1.62 2.35 1.75 4,10 3.57 3.05 3.48 2.98 2.42 2.79 2.17 1.57 2.31 1.67 4,11 3,48 2.99 3.43 2.95 2.40 2.75 2.12 1.54 2.27 1.66 4,13 3,48 2.99 3.43 2.97 2.40 2.75 2.12 1.54 2.27 1.66 4,13 3,48 2.99 3.43 2.97 2.40 2.75 2.12 1.54 2.27 1.66 4,13 3,48 2.99 3.43 2.97 2.40 2.75 2.12 1.54 2.27 1.66 4,13 3,48 2.99 3.43 2.97 2.40 2.75 2.12 1.54 2.27 1.66 6,0 0.90 0.35 -0.36 0.75 0.18 -0.50 1.25 0.42 -0.06 1.35 0.92 0.65 0.98 0.32 -0.38 0.75 0.77 -0.46 1.25 0.42 -0.06 1.40 0.65 0.98 0.32 -0.38 0.78 0.20 -0.46 1.30 0.54 0.04 0.65 1.00 0.46 -0.20 1.08 0.25 -0.20 1.64 0.92 0.38 1.94 0.67 1.00 0.46 -0.20 1.08 0.45 -0.02 1.64 0.92 0.69 1.14 0.60 -0.06 1.26 0.00 1.84 1.14 0.88 1.94 0.70 1.13 0.06 0.00 1.36 0.40 0.48 1.24 0.88 1.94 0.71 1.30 0.66 0.00 1.36 0.84 0.14 1.92 1.22 0.66 2.09 0.72 1.36 0.70 0.16 1.16 0.89 0.12 0.00 1.84 1.14 0.74 1.50 0.90 0.30 0.30 0.30 0.48 1.94 0.75 1.50 0.90 0.30 1.36 0.86 0.90 1.36 0.90 0.74 1.50 0.90 0.30 1.36 0.86 0.30 1.36 0.90 0.75 1.60 0.90 0.30 1.36 0.40 0.48 1.90 1.84 0.88 2.00 1.40 0.68 2.04 1.50 0.84 2.30 1.72 0.88 2.00 1.40 0.68 2.04 1.50 0.84 2.38 1.72 0.89 2.00 1.40 0.68 2.04 1.80 1.20 2.42 1.80 0.80 2.00 1.72 1.80 1.80 1.20 2.42 1.80 0.80 2.00 1.72 1.80 1.80 1.20 2.42 1.80 0.80 2.10 1.72 1.80 1.80 1.20 2.42 1.80 0.80 2.10 1.72 1.80 1.80 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 1.80 1.80 1.80 0.80 2.10 1.80 1.20 2.40 1.80 1.20 2.40 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.8	19U	_	4.27	3.63	3.11	3.64	3.06	2.50	2.88	2.28	1.66	2.43	1.81	2.20	1.58
4,20 3,57 3,06 3,54 2,98 2,42 2,79 2,17 1,157 2,31 1,70 4,18 3,48 2,99 3,48 2,97 2,30 2,66 2,03 1,15 2,27 1,15 2,17 1,15 2,27 1,15 2,27 1,15 2,27 1,15 2,27 2,27 2,17 2,17 2,27 1,15 2,27 1,15 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 2,27 1,25 2,27 2,27 1,25 2,27 1,25 0.01 1,25 0.01 1,26 0.02 0.01 1,26 0.02 0.01 1,26 0.02 0.03 0.04 0.05 0.04 1,26 0.06 1,26 0.02 0.04 1,26 0.06 1,26 0.02 0.04 1,16 0.06 0.06 1,26 0.02 0.04	750		4.24	3.60	3.09	3.58	3.02	2.46	2.83	2.23	1.62	2.35	1.75	2.13	1.53
4,18 3.55 3.05 3.48 2.95 2.40 2.75 2.12 1.54 2.27 1.66 0.57 0.94 0.34 0.36 0.34 0.80 0.19 0.46 1.11 0.38 0.11 1.21 0.58 0.57 0.94 0.35 0.75 0.14 0.80 0.19 0.46 1.11 0.38 0.11 1.21 0.58 0.60 0.90 0.33 0.35 0.75 0.18 0.75 0.15 0.42 0.00 1.35 0.75 0.64 0.98 0.34 0.35 0.75 0.18 0.25 0.46 1.10 0.38 0.04 1.20 0.35 0.75 0.18 0.25 0.46 1.20 0.48 0.04 1.20 0.05 0.04 0.09 0.04 0.03 0.03 0.03 0.03 0.03 0.02 0.04 1.24 0.08 0.25 0.04 1.24 0.08 0.25 0.04 1.20 0.06 1.20 0.09 0.00 0.00 0.00 0.00 0.00 0.00 0	791.		4.20	3.57	3.06	3.54	2.98	2.42	2.79	2.17	1.57	2.31	1.70	2.07	1.47
V 4,13 3,48 2,99 3,43 2,87 2,166 2,03 1,52 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 2,06 1,55 0,17 0,14 0,14 0,14 1,06 0,14 1,06 0,14 1,06 0,14 1,06 0,14 1,06 1,07 0,16 1,16 1,16 0,18 0,14 0,06 1,16 0,16 1,17 0,16 1,17 0,16 1,17 0,17 1,18 0,18 0,14 0,18 0,14 0,18 1,14 0,18 1,19 1,14 0,18 1,14 0,18 1,14 0,18 1,14 0,18 1,14 0,18 1,14 0,18	79Ľ		4.18	3.55	3.05	3.48	2.95	2.40	2.75	2.12	1.54	2.27	1.66	2.04	1.43
0.57 0.94 0.36 -0.34 0.80 0.19 -0.46 1.11 0.38 -0.11 1.21 0.58	790	-	4.13	3.48	2.99	3.43	2.87	2.30	2.66	2.03	1.52	2.06	1.55	1.92	1.30
	080	0.57	0.94	0.36	-0.34	0.80	0.19	-0.46	1.11	0.38	-0.11	1.21	0.58	1.78	1.15
0.60 0.99 0.35 -0.35 0.76 0.18 -0.56 1.15 0.42 -0.06 1.35 0.92 0.61 0.88 0.34 -0.35 0.75 0.17 -0.48 1.24 0.48 -0.04 1.40 1.06 0.62 0.89 0.33 -0.34 0.78 0.27 -0.48 1.24 0.48 -0.04 1.40 1.06 0.65 0.99 0.32 -0.38 0.26 -0.23 1.42 0.70 0.16 1.76 1.25 0.65 0.99 0.32 -0.38 0.26 -0.20 1.08 0.26 -0.20 1.09 0.49 0.39 1.54 0.88 1.87 1.34 0.68 1.06 0.52 -0.16 1.16 0.58 1.04 1.05 0.69 1.14 0.60 -0.20 1.08 0.04 1.76 1.03 0.48 1.99 1.48 1.06 0.00 0.46 0.00 1.36 0.00 1.84 1.14 0.60 0.00 0.46 0.00 1.36 0.00 1.84 1.14 0.60 0.00 0.10 1.36 0.20 1.36 0.00 1.30 0.72 1.36 0.70 0.10 1.46 0.92 0.20 1.30 0.72 1.30 0.48 1.97 1.34 0.88 0.26 0.28 1.87 1.34 0.78 1.34 0.78 1.34 0.78 1.34 0.78 1.34 0.78 1.34 0.78 1.34 0.78 1.58 0.99 0.30 1.55 0.90 0.20 0.20 0.20 0.20 0.20 1.30 0.72 1.36 0.98 0.30 1.70 1.40 0.48 1.28 1.40 0.44 1.80 1.30 0.48 1.30 0.48 1.30 0.48 1.30 0.48 1.30 0.44 1.80 1.25 0.44 1.88 1.28 1.30 1.74 1.88 1.28 1.30 1.74 1.88 1.28 1.30 1.74 1.88 1.28 1.30 1.34 0.34 1.38 1.38 1.38 1.38 1.38 1.38 1.38 1.38	22D	;	1	1	;	;	}	•	}	!	1	1	0.75	1.86	1.25
0.61 0.88 0.34 -0.36 0.75 0.17 -0.48 1.24 0.48 -0.04 1.40 1.06 0.62 0.89 0.32 -0.38 0.25 -0.34 0.80 0.25 -0.34 0.80 0.25 -0.34 0.80 0.25 0.33 -0.34 0.80 0.25 0.33 0.80 0.16 1.16 1.25 0.69 0.40 -0.28 0.94 0.35 -0.28 1.54 0.82 0.28 1.87 1.34 0.68 1.06 0.52 -0.16 1.06 0.54 0.04 1.04 1.05 0.68 1.06 0.50 1.00 0.46 -0.20 1.00 0.45 -0.02 1.00 0.45 1.00 0.46 1.00 0.46 0.00 1.00 1.00 0.40 1.00 0.40 0.00 1.00 0.40 0.4	36D	09.0	06.0	0.35	-0.35	0.76	0.18	-0.50	1.15	0.42	-0.06	1.35	0.92	1.94	1.33
0.62 0.89 0.32 -0.38 0.78 0.2C -0.46 1.30 0.54 0.04 1.66 1.16 0.64 0.92 0.33 -0.34 0.88 0.2b -0.32 1.42 0.70 0.16 1.76 1.25 0.65 0.98 0.40 -0.28 0.94 0.38 1.94 1.40 0.65 1.00 0.46 -0.20 1.08 0.45 -0.20 1.64 0.94 0.38 1.94 1.40 1.66 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 1.90 0.72 1.14 0.60 -0.06 1.2b 0.84 0.14 1.90 1.84 1.14 0.68 1.06 1.36 0.00 1.36 0.04 1.30 0.48 1.99 1.48 1.90 0.72 1.30 0.66 0.00 1.36 0.94 0.18 1.90 0.72 2.03 1.55 0.74 1.50 0.86 0.10 1.46 0.92 0.20 1.30 0.72 2.03 1.55 0.74 1.50 0.86 0.10 1.46 0.92 0.20 1.30 0.72 2.13 1.58 0.76 1.55 0.92 0.30 1.74 1.50 0.86 0.30 1.70 1.20 0.95 0.20 1.30 0.72 2.13 1.80 1.99 1.48 1.99 1.48 1.90 1.25 0.96 0.30 1.74 1.80 1.99 1.48 1.90 1.25 0.96 0.30 1.74 1.80 1.88 1.30 1.72 1.30 1.70 1.44 1.80 1.80 1.30 1.44 1.80 1.30 1.44 1.80 1.30 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.44 1.80 1.20 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.3	50D	0.61	0.88	0.34	-0.36	0.75	0.17	-0.48	1.24	0.48	-0.04	1.40	1.06	1.99	1.39
0.64 0.92 0.33 -0.34 0.88 0.26 -0.32 1.42 0.70 0.16 1.76 1.25 0.65 0.98 0.40 -0.28 0.94 0.35 -0.28 1.54 0.82 0.28 1.87 1.34 0.65 0.08 1.06 0.52 -0.16 1.16 0.58 1.54 0.82 0.28 1.87 1.34 0.69 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 0.69 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 0.72 1.14 0.60 -0.06 1.26 0.64 0.00 1.84 1.14 0.58 2.06 1.52 0.07 0.10 1.14 0.09 0.20 1.36 0.28 2.10 1.34 0.58 2.06 1.55 0.07 0.10 1.46 0.99 0.20 1.36 0.28 2.10 1.36 0.78 2.16 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.64 0.78 1.58 0.78 1.58 0.78 1.58 0.30 1.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.78 1.68 1.08 0.32 1.80 1.25 0.96 2.30 1.74 0.88 1.38 0.62 2.00 1.44 0.76 2.30 1.64 1.08 2.31 1.78 1.89 0.88 2.00 1.40 0.68 2.04 1.50 0.94 2.37 1.70 0.88 1.22 1.48 1.82 1.22 2.44 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.25 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.88 1.25 2.45 1.89 1.24 2.45 1.89	64D	0.62	0.89	0.32	-0.38	0.78	0.20	-0.46	1.30	0.54	0.04	1.66	1.16	7.04	1.44
0.65 0.98 0.40 -0.28 0.94 0.3h -0.28 1.54 0.82 0.28 1.87 1.34 0.67 1.00 0.46 -0.20 1.08 0.45 -0.20 1.64 0.94 0.38 1.94 1.40 0.68 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 0.69 1.14 0.60 -0.06 1.26 0.64 0.00 1.84 1.14 0.58 2.06 1.55 0.70 0.71 1.30 0.66 0.00 1.36 0.84 0.14 1.92 1.22 0.66 2.09 1.55 0.72 1.36 0.70 0.10 1.46 0.92 0.20 2.00 1.30 0.72 2.13 1.58 0.74 1.50 0.92 0.26 1.64 0.94 0.38 2.10 1.36 0.78 2.10 1.50 0.96 2.09 1.55 0.75 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.09 1.55 0.78 1.68 1.08 0.32 1.04 1.20 0.56 2.18 1.50 0.90 2.25 1.64 0.78 1.68 1.08 0.32 1.80 1.20 0.56 2.18 1.50 0.90 2.25 1.64 0.88 2.00 1.34 0.44 1.86 1.40 0.68 2.24 1.60 1.02 2.30 1.74 0.88 2.06 1.44 0.86 2.00 1.40 0.68 2.04 1.00 2.44 1.80 1.22 2.44 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.44 1.86 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.44 1.86 1.24 2.43 1.89 1.24 2.44 1.86 1.24 2.44 1.88 1.24 2.45 1.89 1.24 2.43 1.89 1.24 2.48 1.89 1.24 2.43 1.89 1.24 2.43 1.89 1.24 2.43 1.89 1.24 2.43 1.89 1.24 2.44 1.80 1.24 2.43 1.89 1.24 2.44 1.80 1.24 2.44 1.8	780	0.64	0.92	0.33	-0.34	0.88	0.26	-0.32	1.42	0.70	0.16	1.76	1.25	2.08	1.46
0.67 1.00 0.46 -0.20 1.08 0.45 -0.20 1.64 0.94 0.38 1.94 1.40 0.68 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 1.90 0.69 11.14 0.60 -0.06 1.26 0.64 0.00 1.84 1.14 0.68 2.06 1.52 0.70 0.71 1.30 0.66 0.00 1.36 0.84 0.14 1.92 1.22 0.66 2.09 1.55 0.72 1.36 0.70 0.10 1.46 0.92 0.20 2.00 1.30 0.72 2.13 1.58 0.74 1.50 0.86 0.26 1.62 0.98 2.10 1.36 0.78 2.16 1.61 0.78 1.52 0.98 0.30 1.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.78 1.68 0.32 1.80 1.32 0.68 2.24 1.60 1.02 2.30 1.74 0.88 1.36 0.62 2.00 1.44 0.68 2.24 1.60 1.02 2.30 1.74 0.88 2.06 1.48 0.86 2.20 1.44 0.86 2.30 1.72 1.83 1.78 1.89 1.72 1.04 2.30 1.72 1.08 2.48 1.89 1.22 2.44 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.31 2.51 1.81 2.51 1.81 2.44 1.88 1.25 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.44 1.88 1.25 2.45 1.89 1.24 2.48 1.89 1.24 2.44 1.88 1.25 2.45 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.45 1.89 1.24 2.48 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.44 1.88 1.24 2.44 1.88 1.25 2.44 1.89 1.24 2.48 1.81 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.45 1.89 1.24 2.44 1.89 1.24 2.45 1.89 1.24 2.44 1.89 1.24 2.44 1.89 1.24 2.43 1.89 1.24 2.44 1.89 1.24 1.24	.92D	0.65	0.98	0.40	-0.28	0.94	0.36	-0.28	1.54	0.82	0.28	1.87	1.34	2.11	1.51
0.68 1.06 0.52 -0.16 1.16 0.58 -0.04 1.76 1.03 0.48 1.99 1.48 0.69 1.14 0.60 -0.06 1.26 0.64 0.00 1.84 1.14 0.58 2.06 1.52 0.71 1.30 0.66 0.00 1.36 0.92 0.20 1.32 0.65 2.09 1.55 0.72 1.36 0.70 0.10 1.46 0.92 0.20 1.30 0.72 2.13 1.58 0.74 1.50 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.55 0.75 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.64 0.70 0.70 1.20 0.55 2.10 1.36 0.78 2.16 1.61 0.70 0.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.70 0.78 1.68 1.08 0.32 1.80 1.25 0.56 2.18 1.54 0.94 2.27 1.70 0.83 1.86 1.36 0.62 2.00 1.44 0.76 2.30 1.74 1.86 1.70 0.76 1.56 0.98 2.04 1.50 0.94 2.27 1.70 0.88 2.06 1.48 0.80 2.12 1.64 0.96 2.42 1.78 1.18 2.43 1.87 2.12 1.56 0.86 2.20 1.64 1.88 1.22 2.44 1.88 1.22 2.44 1.88 1.25 2.45 1.83 1.24 2.48 1.89 1.25 2.44 1.88 1.25 2.45 1.87 1.28 2.44 1.88 1.25 2.45 1.87 1.28 2.44 1.88 1.25 2.45 1.87 1.28 2.44 1.88 1.25 2.46 1.89 1.24 2.44 1.86 1.25 2.46 1.89 1.24 2.44 1.86 1.25 2.46 1.89 1.24 2.44 1.88 1.25 2.46 1.89 1.24 2.44 1.88 1.25 2.45 1.87 1.28 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.45 1.87 1.28 2.45 1.87 1.28 2.45 1.87 1.28 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.25 2.45 1.87 1.28 2.45 1.83 1.24 2.43 1.83 1.24 2.43 1.83 1.24 2.43 1.83 1.24 2.43 1.83 1.24 2.44 1.88 1.25 2.45 1.87 1.28 2.45 1.83 1.24 2.44 1.85 1.25 2.45 1.87 1.83 1.24 2.43 1.83 1.24 2.43 1.83 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.83 1.24 2.43 1.83 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.88 1.25 2.45 1.83 1.24 2.44 1.83 1.24 2.44 1.88 1.25 2.44 1.88 1.24 2.44 1.88 1.25 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.88 1.24 2.44 1.	.06р	0.67	1.00	97.0	-0.20	1.08	0.45	-0.20	1.64	0.94	0.38	1.94	1.40	2.15	1.55
0.69 1.14 0.60 -0.06 1.26 0.64 0.00 1.84 1.14 0.58 2.06 1.52 0.71 1.30 0.66 0.00 1.36 0.84 0.14 1.92 1.22 0.66 2.09 1.55 0.72 1.36 0.70 0.10 1.46 0.92 0.20 2.00 1.30 0.72 2.13 1.58 0.74 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.64 0.75 1.52 0.93 0.30 1.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.78 1.68 1.08 0.32 1.80 1.25 0.56 2.18 1.54 0.94 2.27 1.70 0.83 2.06 1.48 0.62 2.00 1.44 0.76 2.30 1.66 1.08 2.33 1.78 0.88 2.06 1.48 0.80 2.12 1.56 0.94 2.42 1.89 1.87 0.88 2.06 1.48 0.80 2.12 1.56 0.94 2.42 1.89 1.87 2.30 1.72 1.04 2.30 1.72 1.08 2.44 1.88 1.22 2.48 1.89 1.30 2.49 1.90 2.44 1.88 1.25 2.44 1.88 1.25 2.44 1.88 1.25 2.50 1.83 1.24 2.47 1.87 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.24 2.47 1.81 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.25 2.45 1.83 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.25 2.45 1.81 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.24 2.43 1.83 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.24 2.43 1.83	20D	0.68	1.06	0.52	-0.16	1.16	0.58	-0.04	1.76	1.03	0.48	1.99	1.48	2.19	1.58
0.71 1.30 0.66 0.00 1.36 0.84 0.14 1.92 1.22 0.66 2.09 1.55 0.72 1.36 0.70 0.10 1.46 0.92 0.20 2.00 1.30 0.72 2.13 1.58 0.74 1.50 0.86 0.12 1.52 0.96 0.28 2.10 1.36 0.78 2.16 1.61 0.75 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.64 0.78 1.68 1.08 0.32 1.80 1.20 0.55 2.16 1.50 0.90 2.25 1.67 0.78 1.68 1.08 0.32 1.80 1.40 0.68 2.24 1.60 1.02 2.37 1.70 0.83 1.86 1.36 0.62 2.00 1.44 0.76 2.30 1.66 1.08 2.33 1.78 0.86 2.00 1.40 0.68 2.04 1.50 0.84 2.38 1.72 1.12 2.37 1.83 0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 2.30 1.72 1.04 2.30 1.72 1.08 2.50 1.88 1.20 2.49 1.80 2.46 1.88 1.26 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.90 1.28 2.50 1.87 1.31 2.51 1.91 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.85 1.25 2.45 1.83 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.85 1.25 2.45 1.83 2.44 1.86 1.25 2.45 1.89 1.24 2.48 1.83 1.24 2.43 1.83 2.44 1.86 1.25 2.45 1.89 1.24 2.48 1.83 1.24 2.43 1.83	34D	69.0	1.14	09.0	-0.06	1.26	0.64	0.00	1.84	1.14	0.58	2.06	1.52	2.21	1.62
0.72	48D	0.71	1.30	0.66	0.00	1.36	0.84	0.14	1.92	1.22	0.66	2.09	1.55	2.23	1.63
0.74 1.50 0.86	62D	0.72	1.36	0.70	0.10	1.46	0.92	0.20	2.00	1.30	0.72	2.13	1.58	2.25	1.67
0.75 1.52 0.92 0.26 1.62 1.04 0.48 2.12 1.42 0.86 2.20 1.64 0.76 1.56 0.98 0.30 1.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.78 1.58 0.98 0.30 1.70 1.20 0.55 2.16 1.50 0.90 2.25 1.67 0.78 1.68 1.08 0.32 1.80 1.25 0.68 2.24 1.60 1.02 2.30 1.74 0.83 1.86 1.36 0.68 2.00 1.44 0.76 2.30 1.64 1.00 2.30 1.74 0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 1.89 2.12 1.56 0.86 2.20 1.64 1.00 2.44 1.80 1.22 2.48 1.89 1.20 2.40 1.90 2.44 1.88 1.26 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.44 1.88 1.26 2.45 1.89 1.24 2.45 1.87 1.81 2.51 1.91 2.51 1.81 2.44 1.88 1.26 2.45 1.89 1.24 2.48 1.89 1.24 2.45 1.85 2.44 1.86 1.25 2.45 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.83 1.24 2.43 1.83 1.24 2.45 1.85	76D	0.74	1.50	۰.86	٥.12	1.52	96.0	0.28	2.10	1.36	0.78	2.16	1.61	2.28	1.69
0.76 1.56 0.98 0.30 1.70 1.20 0.52 2.16 1.50 0.90 2.25 1.67 0.78 1.68 1.08 0.32 1.80 1.25 0.56 2.18 1.54 0.94 2.27 1.70 0.81 1.80 1.34 0.44 1.86 1.40 0.68 2.24 1.60 1.02 2.30 1.74 0.88 2.06 1.49 0.68 2.00 1.44 0.76 2.30 1.66 1.08 2.33 1.78 1.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.82 2.43 1.87 2.42 1.70 2.30 1.72 1.90 2.48 1.89 2.44 1.88 1.22 2.44 1.88 1.26 2.44 1.88 1.26 2.44 1.88 1.26 2.44 1.89 1.26 2.48 1.87 1.31 2.31 1.91 2.47 1.89 2.44 1.88 1.26 2.45 1.87 1.87 1.87 1.88 2.44 1.88 1.26 2.45 1.87 1.87 1.87 1.87 1.87 1.88 2.44 1.88 1.26 2.45 1.89 1.24 2.48 1.87 1.87 1.87 1.87 2.47 1.89 2.45 1.89 1.24 2.48 1.87 1.25 2.45 1.87 1.81 2.41 1.88 1.26 2.45 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.89 1.24 2.48 1.83 1.24 2.43 1.83 1.24 2.43 1.83 1.24 2.44 1.88 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	006	0.75	1.52	0.92	0.26	1.62	1.04	0.48	2.12	1.42	0.86	2.20	1.64	2.31	1.71
0.78	.04D	0.76	1.56	0.98	0.30	1.70	1.20	0.52	2.16	1.50	0.00	2.25	1.67	2.33	1.74
0.81 1.80 1.34 0.44 1.86 1.40 0.68 2.24 1.60 1.02 2.30 1.74 0.83 1.86 1.36 0.62 2.00 1.44 0.76 2.30 1.66 1.08 2.33 1.78 0.88 2.00 1.40 0.68 2.04 1.50 0.84 2.38 1.72 1.12 2.37 1.83 0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 2.12 1.56 0.86 2.20 1.64 1.00 2.44 1.80 1.22 2.48 1.89 2.46 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.92 1.34 2.54 1.87 1.31 2.51 1.91 2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.83 1.24 2.43 1.83 2.44 1.86 1.25 2.45 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.18D	0.78	1.68	1.08	0.32	1.80	1.25	0.56	2.18	1.54	0.94	2.27	1.70	2.36	1.76
0.83	.46	0.81	1.80	1.34	0.44	1.86	1.40	0.68	2.24	1.60	1.02	2.30	1.74	2.40	1.80
0.86 2.00 1.40 0.68 2.04 1.50 0.84 2.38 1.72 1.12 2.37 1.83 0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 2.12 1.56 0.86 2.20 1.64 1.00 2.44 1.80 1.22 2.48 1.89 2.30 1.72 1.04 2.30 1.72 1.08 2.48 1.83 1.24 2.48 1.89 2.46 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.46 1.88 1.26 2.60 1.90 1.28 2.50 1.88 1.30 2.49 1.90 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.85 1.25 2.45 1.87 2.44 1.86 1.25 2.45 1.89 1.24 2.48 1.83 1.24 2.43 1.83 2.44 1.86 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.74D	0.83	1.86	1.36	0.62	2.00	1.44	0.76	2.30	1.66	1.08	2.33	1.78	2.45	1.85
0.88 2.06 1.48 0.80 2.12 1.56 0.96 2.42 1.78 1.18 2.43 1.87 2.12 1.56 0.86 2.20 1.64 1.00 2.44 1.80 1.22 2.48 1.89 2.30 1.72 1.04 2.30 1.72 1.08 2.48 1.83 1.24 2.48 1.89 2.49 1.80 2.47 1.90 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.90 1.28 2.50 1.87 1.31 2.51 1.91 2.44 1.88 1.26 2.45 1.89 1.26 2.50 1.87 1.25 2.45 1.87 1.87 1.28 2.45 1.89 2.50 1.85 1.25 2.45 1.85 2.45 1.89 1.24 2.48 1.85 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.02D	0.86	2.00	1.40	0.68	2.04	1.50	0.84	2.38	1.72	1.12	2.37	1.83	2.50	1.88
2.12 1.56 0.86 2.20 1.64 1.00 2.44 1.80 1.22 2.48 1.89 2.30 1.72 1.04 2.30 1.72 1.08 2.48 1.83 1.24 2.48 1.89 2.46 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.92 1.34 2.54 1.87 1.31 2.51 1.91 2.54 1.88 1.26 2.46 1.89 1.26 2.46 1.89 1.26 2.45 1.87 1.28 2.47 1.87 2.44 1.86 1.25 2.45 1.89 1.24 2.50 1.85 1.25 2.45 1.83 1.24 2.48 1.89 1.24 2.48 1.83 1.24 2.43 1.83 1.24 2.48 1.83 1.24 2.43 1.83	300	0.88	2.06	1.48	08.0	2.12	1.56	96.0	2.42	1.78	1.18	2.43	1.87	2.53	1.92
2.30 1.72 1.04 2.30 1.72 1.08 2.48 1.83 1.24 2.48 1.89 2.46 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.92 1.34 2.54 1.87 1.31 2.51 1.91 2.46 1.88 1.26 2.46 1.90 1.28 2.52 1.87 1.28 2.47 1.87 2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 2.44 1.86 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.580		2.12	1.56	0.86	2.20	1.64	1.00	5.44	1.80	1.22	2.48	1.89	2.52	1.92
2.46 1.88 1.22 2.44 1.88 1.28 2.50 1.88 1.30 2.49 1.90 2.47 1.90 1.28 2.50 1.92 1.34 2.54 1.87 1.31 2.51 1.91 2.46 1.88 1.26 2.46 1.90 1.28 2.52 1.87 1.28 2.47 1.87 2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 2.44 1.86 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.86D	_	2.30	1.72	1.04	2.30	1.72	1.08	2.48	1.83	1.24	2.48	1.89	2.52	1.92
2.47 1.90 1.28 2.50 1.92 1.34 2.54 1.87 1.31 2.51 1.91 2.46 1.88 1.26 2.46 1.90 1.28 2.52 1.87 1.28 2.47 1.87 2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 2.44 1.86 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.80D		2.46	1.88	1.22	2.44	1.88	1.28	2.50	1.88	1.30	5.49	1.90	2.52	1.92
2.46 1.88 1.26 2.46 1.90 1.28 2.52 1.87 1.28 2.47 1.87 1.87 2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 1.26 2.48 1.85 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.40D		2.47	1.90	1.28	2.50	1.92	1.34	2.54	1.87	1.31	2.51	1.91	2.53	1.92
2.44 1.86 1.25 2.45 1.89 1.26 2.50 1.85 1.25 2.45 1.85 1.85 1.85 1.85 1.85 1.85 1.85 1.8	. 60D		2.46	1.88	1.26	2.16	1.90	1.28	2.52	1.87	1.28	2.47	1.87	5.49	1.89
) V 2.44 1.86 1.24 2.43 1.88 1.24 2.48 1.83 1.24 2.43 1.83	.15D		2.44	1.86	1.25	2.45	1.89	1.26	2.50	1.85	1.25	2.45	1.85	2.47	1.87
	. 70D	-	5.44	1.86	1.24	2.43	1.88	1.24	2.48	1.83	1.24	2.43	1.83	2.45	1.85

Table 4 Average Piezometer Readings, Type 3 Expansion

В	Piezometer locations	ations						Run Number*	ber*					
No.	Station	Elevation	240	241	242	243	244	245	246	247	248	249	250	251
4	15.00U	0.56	4.73	5.37	3.69	3.48	4.12	4.65	4.55	3.92	3.67	4.42	4.79	4.41
Ŋ	8.790	_	4.68	5.31	3.66	3.42	4.06	4.58	47.44	3.84	3.53	4.28	4.65	4.30
9	6.750		4.67	5.30	3.65	3.41	4.04	4.57	4.42	3.82	3.50	4.26	4.62	4.28
7	4.790		4.66	5.29	3.65	3.40	4.03	4.56	4.41	3.81	3.48	4.24	4.61	4.26
œ	2.79U		4.64	5.28	3.64	3.39	4.03	4.55	4.40	3.80	3.47	4.22	4.59	4.26
6	1.790		4.64	5.26	3.63	3.37	4.01	4.53	4.38	3.77	3.44	4.19	4.55	4.23
14	0.070		0.38	0.82	0.84	0.39	1.08	1.59	-0.02	0.13	-0.15	0.56	1.20	1.43
15	0.180		0.38	0.82	0.84	0.37	1.07	1.58	-0.02	0.12	-0.16	0.55	1.20	1.42
16	0.330	_	0.37	0.82	0.84	0.36	1.07	1.58	-0.02	0.12	-0.16	0.55	1.19	1.41
17	0.470	0.58	0.36	0.82	0.84	0.36	1.07	1.57	-0.03	0.12	-0.16	0.55	1.18	1.41
18	0.61D	0.59	0.36	ŧ	;	0.36	1.06	1.57	-0.03	0.11	-0.16	0.55	1.17	1.40
19	0.750	0.61	0.36	0.81	0.82	0.36	1.05	1.57	-0.03	0.11	-0.16	0.57	1.19	1.41
20	0.890	0.62	0.36	0.82	0.83	0.37	1.06	1.56	-0.02	0.11	-0.13	0,00	1.22	1.43
21	1.030	0.63	0.38	0.82	0.83	0.39	1.07	1.58	0.00	0.12	-0.10	0.64	1.24	1.46
22	1.17D	0.65	0.38	0.83	0.84	0.39	1.09	1.60	0.02	0.14	-0.07	0.67	1.27	1.49
23	1.315	0.66	0.40	0.84	0.85	0.41	1.10	1.62	0.05	0.17	0.00	0.70	1.32	1.55
54	1.45D	0.68	0.41	0.85	0.85	0.45	1.12	1.64	0.07	0.18	0.05	0.76	1.37	1.61
25	1.590	0.69	0.42	0.87	0.86	0.47	1.15	1.66	0.11	0.20	0.10	0.01	1.43	1.65
56	1.73D	0.70	0.44	0.88	0.88	0.50	1.18	1.68	0.15	0.25	0.17	0.00	1.49	1.71
27	1.870	0.72	0.46	0.90	0.90	0.52	1.22	1.70	0.20	0.30	0.23	0.95	1.56	1.77
28	2.01D	0.73	0.50	0.94	0.91	0.55	1.24	1.73	0.25	0.33	0.29	1.01	1.62	1.81
59	2.15D	0.75	0.52	0.97	0.93	0.60	1.28	1.78	0.30	0.37	0.38	1.09	1.67	1.86
30	2.29D	0.76	0.57	1.00	96.0	0.62	1.32	1.81	0.33	0.40	0.44	1.15	1.73	1.91
31	2.43D	0.77	0.61	1.02	0.97	0.65	1,35	1.83	0.37	0.44	0.51	1.21	1.79	1.94
32	2.71D	0.80	99.0	1.04	1.01	0.69	1.40	1.85	0.44	0.52	0.57	1.30	1.85	2.03
33	2.990	0.83	0.70	1.12	1.04	0.76	1.45	1.90	0.53	0.58	0.68	1.39	1.95	5.09
34	3.270	0.86	0.74	1.20	1.06	0.85	1.52	1.94	0.61	0.65	0.78	1.48	7.04	2.13
35	3.55D	0.88	0.79	1.28	1.10	0.00	1.60	2.00	0.75	0.80	0.88	1.57	2.15	2.20
36	3.83D		0.90	1.32	1.19	1.00	1.63	2.11	0.82	0.85	1.00	1.65	2.25	2.26
37	4.11D		96.0	1.40	1.24	1.05	1.70	2.20	0.94	0.91	1.09	1.75	2.35	2.35
38	5.050	_	1.22	1.67	1.40	1.20	1.89	2.40	1.15	1.10	1.20	1.87	2.45	2.46
39	6.65D		1.22	1.72	1.41	1.25	1.91	2.42	1.24	1.16	1.23	1.95	2.50	5.49
0,4	8.040		1.22	1.72	1.41	1.24	1.90	2.41	1.23	1.16	1.22	1.94	2.48	2.48
41	009.6		1.22	1.72	1.40	1.23	1.90	2.41	1.23	1.16	1.22	1.93	2.46	2.48
42	11.15D		1.22	1.72	1.40	1.23	1.90	2.41	1.23	1.16	1.22	1.9.	2.46	2.47
43	12.70D	-	1.22	1.72	1.40	1.22	1.90	2.40	1.22	1.15	1.21	1.91	2.45	2.47
						(Continued)	nued)							

* Refer to Table 1 for flow conditions for each run.

Table 4 (Continued)

	262	2.86	2.60	2.51	2.50	2.45	2.33	-0.94	-0.94	-0.93	-0.92	-0.86	-0.75	-0.64	-0.49	-0.37	-0.24	-0.12	0.02	0.13	0.24	0.35	0.44	0.52	0.61	0.69	0.81	0.92	1.04	1.15	1.21	1.31	1.32	1.30	1.28	1.27	1.25
	261	2.69	2.46	2.41	2.37	2.34	2.25	-0.67	-0.68	-0.67	-0.66	-0.62	-0.51	-0.43	-0.31	-0.20	-0.10	0.05	0.18	0.30	0.40	0.49	0.55	0.62	0.71	0.79	0.86	0.96	1.03	1.10	1.20	1.28	1.30	1.28	1.27	1.25	1.24
	260	3.61	3.41	3.36	3.32	3.30	3.21	0.86	0.87	0.88	0.90	0.93	0.98	1.09	1.20	1.30	1.40	1.51	1.58	1.65	1.71	1.77	1.83	1.90	1.96	2.06	2.15	2.24	2.29	2.34	2.37	2.46	2.47	2.46	2.44	2.43	2.42
	259	3.20	2.97	2.92	2.87	2.85	2.75	0.17	0.13	0.15	0.18	0.23	0.30	0.40	0.51	0.62	0.76	0.88	0.98	1.09	1.19	1.26	1.32	1.37	1.44	1.52	1.62	1.70	1.80	1.87	1.90	1.92	1.93	1.92	1.90	1.88	1.87
	258	2.55	2.34	2.30	2.26	2.23	2.14	-0.46	-0.46	-0.45	-0.43	-0.40	-0.35	-0.30	-0.17	-0.07	0.06	0.17	0.27	0.38	0.49	0.57	0.63	0.73	0.78	78.0	0.93	1.07	1.14	1.20	1.25	1.32	1.32	1.32	1.30	1.28	1.27
Run Number	257	3.92	3.68	3.63	3.59	3.56	3.48	-0.83	-0.84	-0.85	-0.85	-0.85	-0.78	-0.70	-0.64	-0.55	-0.44	-0.28	-0.16	-0.04	0.05	0.14	0.24	0.34	0.43	0.55	0.70	0.85	0.98	1.10	1.20	1.36	1.39	1.37	1.36	1.35	1, 33
	256	3.76	3.50	3.46	3.42	3.39	3.30	-0.63	-0.64	-0.65	-0.65	-0.65	-0.61	-0.57	-0.49	-0.40	-0.29	-0.15	-0.03	90.0	0.14	0.23	0.34	0.42	0.50	0.61	0.78	0.91	1.08	1.21	1.28	1.37	1.38	1.37	1.36	1.35	1.33
	255	4.46	4.26	4.22	4.20	4.18	4.12	1.06	1.05	1.05	1.05	1.06	1.10	1.15	1.20	1.27	1.34	1.41	1.48	1.55	1.65	1.73	1.82	1.92	2.02	2.15	2.26	2.32	2.46	2.52	2.56	2.62	2.62	2.61	2.60	2.60	2,58
	254	3.92	3.72	3.68	3.66	3.64	3.57	0.47	0.46	0.45	0.45	0.45	0.47	0.51	09.0	0.67	0.76	0.84	0.91	0.99	1.06	1.17	1.28	1.36	1.45	1.55	1.64	1.71	1.80	1.90	1.97	2.05	2.08	2.06	2.05	2.05	2.03
	253	3.18	2.97	2.93	2.90	2.88	2.84	-0.36	-0.37	-0.38	-0.39	-0.40	-0.36	-0.32	-0.22	-0.15	-0.06	0.03	0.10	0.20	0.29	0.38	0.47	0.54	0.65	0.78	0.87	0.93	1.02	1.16	1.23	1.26	1.28	1.26	1.24	1.24	1.23
	252	4.10	3.95	3.92	3.90	3.88	3.83	-0.27	-0.27	-0.28	-0.29	-0.30	-0.29	-0.27	-0.22	-0.15	-0.08	-0.03	0.05	0.11	0.19	0.26	0.31	0.37	0.43	0.51	0.59	0.68	0.78	0.90	1.03	1.25	1.32	1.31	1.30	1.30	1.28
ations	Elevation	0.56			-					-	0.58	0.59	0.61	0.62	0.63	0.65	0.66	0.68	0.69	0.70	0.72	0.73	0.75	0.76	0.77	0.80	0.83	0.86	0.88								-
Piezometer Locations	Station	15.00U	8.790	6.750	4.790	2.790	1.790	0.070	0.18D	0.330	0.470	0.61D	0.750	0.890	1.03D	1.17D	1.31D	1.45D	1.590	1.730	1.87D	2.01D	2.15D	2.290	2.430	2.71D	2.99D	3.27D	3.550	3.830	4.11D	5.05D	6.65D	8.04D	009.6	11.150	12 700
12	No.	7	Ŋ	9	7	œ	6	14	15	16	17	18	19	70	21	22	23	54	25	76	2.7	28	29	30	31	3.2	33	34	35	36	37	38	39	07	41	4.2	۲7

Table 4 (Concluded)

P.	Piezometer Locations	ations						Run Number					
Š.	Station	Elevation	263	797	265	266	267	268	269	270	271	272	273
7	15.00U	0.56	1.86	2.45	3.02	1.90	2.19	2.64	2.04	1.91	2.51	1.90	2.13
5	8.79U		1.63	2.24	2.81	1.66	1.86	2.36	1.81	1.60	2.22	1.57	1.76
9	6.750		1.58	2.18	2.76	1.61	1.78	2.31	1.77	1.53	2.15	1.51	1.69
7	4.790		1.54	2.13	2.72	1.57	1.71	2.26	1.73	1.47	2.11	1.45	1.63
œ	2.790		1.51	2.11	2.69	1.53	1.67	2.22	1.71	1.43	2.08	1.42	1.59
6	1.790		1.41	2.02	2.60	1.44	1.53	2.11	1.62	1.31	1.95	1.30	1.45
14	0.07D		-0.25	0.45	1.01	-0.35	-0.95	1.02	0.75	60.0	1.78	1.09	1.25
15	0.18D		-0.25	0.45	1.00	-0.34	-0.95	1.25	0.94	0.37	1.75	1.07	1.23
16	0.330	-	-0.18	0.53	1.08	-0.28	-0.86	1.51	1.12	0.65	1.83	1.15	1.31
17	0.470	0.58	-0.09	0.61	1.15	-0.18	-0.77	1.66	1.23	0.86	1.91	1.24	1.46
18	0.610	0.59	-0.02	0.70	1.25	-0.08	-0.61	1.76	1.33	96.0	1.94	1.27	1.44
19	0.75D	0.61	0.10	0.80	1.37	90.0	-0.45	1.85	1.40	i.05	2.03	1.38	1.54
20	0.890	0.62	0.23	0.93	1.48	0.18	-0.30	1.92	1.45	1.14	2.07	1.41	1.58
21	1.030	0.63	0.37	1.02	1.60	0.31	-0.12	1.97	1.50	1.20	2.11	1.45	1.62
22	1.170	0.65	0.45	1.13	1.70	0.43	0.04	2.02	1.55	1.25	2.15	1.49	1.67
23	1.31D	99.0	0.56	1.22	1.78	0.53	0.19	2.05	1.58	1.30	2.18	1.52	1.71
54	1.45D	0.68	0.65	1.31	1.84	0.62	0.36	2.09	1.61	1.35	2.22	1.56	1.75
25	1.590	69.0	0.71	1.39	1.89	0.68	0.46	2.13	1.64	1.39	2.25	1.59	1.79
56	1.730	0.70	0.77	1.44	1.96	0.76	0.58	2.16	1.66	1.43	2.28	1.62	1.82
27	1.870	0.72	0.84	1.48	2.03	0.83	99.0	2.19	1.68	1.46	2.31	1.65	1.85
28	2.01D	0.73	0.90	1.52	2.08	0.88	0.74	2.22	1.70	1.49	2.33	1.68	1.88
59	2.15D	0.75	0.95	1.58	2.13	0.92	08.0	2.24	1.72	1.52	2.35	1.70	1.91
30	2.29D	0.76	1.00	1.62	2.17	96.0	0.86	2.28	1.74	1.55	2.37	1.73	1.94
31	2.430	0.77	1.03	1.68	2.20	1.00	0.94	2.30	1.76	1.57	2.39	1.75	1.97
32	2.71D	0.80	1.10	1.73	2.25	1.06	1.00	2.35	1.80	1.63	2.44	1.80	2.02
33	2.99D	0.83	1.15	1.78	2.30	1.13	1.07	2.39	1.84	1.67	2.48	1.84	2.06
34	3.27D	0.86	1.21	1.82	2.35	1.19	1.14	2.42	1.88	1.73	2.52	1.89	2.11
35	3.550	0.88	1.25	1.86	2.40	1.24	1.22	2.45	1.93	1.78	2.53	1.93	2.15
36	3.83D		1.28	1.89	2.45	1.27	1.26	2.46	1.93	1.79	2.53	1.92	2.15
37	4.11D		1.30	1.90	2.47	1.30	1.28	2.47	1.92	1.79	2.53	1.92	2.15
38	5.05D		1.31	1.92	2.50	1.32	1.33	2.48	1.92	1.80	;	1.92	2.15
39	6.65D	_	1.32	1.94	2.51	1,33	1.35	2.48	1.92	1.80	;	1.92	2.15
70	8.04D		1.30	1.92	2.50	1.31	1.33	2.46	1.91	1.78	;	1.90	2.14
41	009.6		1.29	1.91	2.48	1.30	1.31	2.44	1.90	1.76	;	1.89	2.13
75	11.150		1.27	1.89	2.47	1.28	1.29	2.43	1.88	1.74	2.51	1.87	2.11
43	12.70D	-	1.26	1.87	2.45	1.26	1.27	2.42	1.87	1.73	5.49	1.86	5.09

Table 5

Average Piezometer Readings, Type 4 Expansion

	290 291	3.69	_											_		_		_			_			_							_		.45 1.26		
	289 2	7	7	7	7	-1	(-)		_		_						-		~	_					6.4	(-1	C	(4	6.4	(4	. 4	• •	. 4	(4	
	288	3.10	2.94	2.91	2.89	2.87	2.82	-0.23	-0.24	-0.25	-0.26	-0.26	-0.25	-0.22	-0.15	-0.08	0.00	0.06	0.14	0.28	0.40	0.55	0.67	0.78	0.88	0.98	1.07	1.15	1.23	1.26	1.26	1.26	1.24	1.23	1.21
	287	3.97	3.86	3.84	3.82	3.80	3.75	-0.31	-0.32	-0.33	-0.34	-0.35	-0.35	-0.34	-0.32	-0.26	-0.22	-0.13	-0.03	0.05	0.09	0.15	0.24	0.45	0.58	0.78	0.91	1.03	1.15	1.29	1.30	1.29	1.28	1.27	1.26
	286	4.32	4.21	4.19	4.17	4.16	4.12	1.35	1.34	1.33	1.33	1.32	1.32	1.33	1.35	1.38	1.41	1.45	1.51	1.57	1.64	1.71	1.76	1.85	1.93	2.08	2.23	2.37	2.44	2.46	2.47	5.46	5.45	77.7	2.43
	285	4.65	4.55	4.53	4.51	4.50	97.7	1.17	1.16	1.15	1.14	1.14	1.15	1.17	1.19	1.23	1.26	1.30	1.38	1.42	1.48	1.55	1.62	1.75	1.88	2.05	2.20	2.32	2.41	5.49	2.50	5.49	2.48	2.48	2.46
er*	283	3.66	3.54	3.53	3.51	3.49	3.45	-0.17	-0.17	-0.18	-0.19	-0.20	-0.20	-0.20	-0.18	-0.13	-0.07	-0.01	0.04	0.10	0.16	0.24	0.30	0.45	0.55	0.70	0.90	1.05	1.15	1.24	1.26	1.26	1.25	1.24	1.24
Run Number*	282	3.77	3.70	3.69	3.68	3.67	3.65	0.15	0.14	0.14	0.13	0.13	0.13	0.12	0.13	0.14	0.15	0.16	0.18	0.20	0.25	0.30	0.36	0.42	0.55	0.69	0.82	0.97	1.10	1.21	1.24	1.24	1.23	1.23	1.22
	281	4.36	4.27	4.26	4.24	4.23	4.21	-0.03	-0.03	-0.04	-0.04	-0.05	-0.05	-0.05	-0.04	-0.03	-0.02	0.00	0.05	0.08	0.12	0.16	0.21	0.30	0.45	0.58	0.75	0.00	1.05	1.25	1.28	1.28	1.27	1.26	1.25
	280	4.45	4.40	4.39	4.38	4.37	4.36	1.60	1.59	1.58	1.57	1.56	1.56	1.56	1.56	1.57	1.58	1.59	1.63	1.65	1.68	1.72	1.76	1.82	1.94	5.06	2.16	2.26	2.35	2.43	5.44	2.44	2.44	2.43	2.43
	279	4.02	3.96	3.95	3.94	3.93	3.91	0.93	0.93	0.92	0.92	0.91	0.92	0.92	0.93	0.93	0.94	0.95	0.97	0.99	1.04	1.07	1.10	1.20	1.29	1.41	1.56	1.65	1.78	1.84	1.86	1.85	1.84	1.84	1.83
	278	3.51	3.45	3.44	3.42	3.41	3.39	0.30	0.30	0.29	0.28	0.27	0.27	0.27	0.27	0.28	0.29	0.30	0.33	0.35	0,40	0.44	0.50	09.0	0.69	0,85	0.95	1.04	1,14	1,23	1.25	1.24	1.25	1,24	1,23
	277	3.72	3.68	3.68	3.67	3.66	3.65	0.72	0.72	0.72	0.72	0.71	0.71	0.71	0.71	0.72	0.72	0.73	0.74	0.75	0.77	0.79	18.0	0.85	06.0	96.0	1.05	1.16	1.25	1.38	1.40	1.40	1.40	1.40	1.40
	275	5.22	5.18	5.17	5.16	5.15	5.14	0.85	0.84	0.84	0.83	0.82	0.82	0.83	0.85	0.87	0.88	0.40	0.94	0.45	0.98	1.02	1.05	1.15	1.23	1.34	1.45	1.58	1.66	1.82	1.85	1.85	1.85	1.84	1.84
	274	4.82	4.77	4.76	4.75	7.74	4.73	0.16	0.15	0.14	0.13	0.13	0.14	0.14	0.15	0.15	0.16	0.16	0.18	0.20	0.23	0.25	0.30	0.37	0.45	0.57	0.73	06.0	1.04	1.19	1.20	1.20	1.20	1.20	1.20
cations	Elevation	0.56					-	0.57	0.58	0.69	0.61	0.62	79.0	0.65	0.67	0.68	69.0	0.71	0.72	_		<u> </u>										_			>
Piezometer Locations	Station	15.00U	8.790	6.750	4.79U	2.79U	1.790	0.080	0.22D	0.36D	0.500	0.64D	0.780	0.92D	1.06D	1.20D	1.340	1.480	1.62D	1.76D	1.900	2.04D	2.18D	2,460	2.74D	3.020	3.30D	3.580	3.860	4.80D	6.40D	8.040	0.40D	11.150	12.70D
Pie	No.	à	5	9	7	&	6	14	15	16	17	18	19	20	7.1	:1	13	70	25	56	7.7	28	67	30	31	32	33	34	35	36	37	38	39	70	- -

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(Continued)

* Refer to Table 1 for flow conditions for each run.

Table 5 (Concluded)

	308	2.58	2.28	2.21	2.14	2.11	1.99	1.78	1.90	1.97	5.06	2.10	2.13	5.19	2.23	2.28	2.32	2.37	2.47	2,41	2.41	2.40	2.40	2.39	2.38	2.38	2.37	2.36	2,35	2.34	2,33	2.31	2.27	2.26	2.22
	307		•	•	•						•	•	•				•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	. •	•
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-	299																																		
Ru	298	2.08	1.87	1.82	1.78	1.76	1.66	0.05	0.05	0.08	0.17	0.23	0.31	0.41	0.52	0.65	0.76	0.85	0.92	1.03	1.10	1.15	1.19	1.23	1.27	1.30	1.32	1.33	1.34	1.35	1.33	1.31	1.27	1.26	1.23
	297	3.06	2.81	2.76	2.71	2.69	2.60	-0.70	-0.70	-0.70	-0.68	-0.61	-0.55	-0.44	-0.34	-0.23	-0.15	-0.02	0.12	0.23	0.36	0.52	0.64	0.80	0.96	1.07	1.17	1.25	1.31	1.33	1.33	1.31	1.26	1.25	1.22
	296	2.86	2.63	2.60	2.58	2,57	2.44	-0.48	-0.49	-0.47	-0.43	-0.39	-0,32	-0,21	-0.12	0.00	0.09	0.20	0.31	0.40	0.52	0.62	0.72	0.84	96.0	1.07	1.16	1.23	1.27	1.33	1,33	1,32	1.28	1.28	1.24
	295	3.87	3.67	3.63	3.59	3.56	3.48	0.97	0.97	0.98	1.01	1.05	1.10	1.16	1,23	1.32	1.40	1.51	1.63	1.74	1.84	1.93	2.05	2.16	2.28	2.41	2.45	2.49	2.52	2.54	2.54	2.53	2.51	2.50	2.48
	294	3.19	3.00	2.96	2.91	2.89	2.81	0.45	0.41	0.41	0.41	0.44	0.50	09.0	0.70	0.78	0.89	1.00	1.09	1.19	1.28	1.36	1.47	1.58	1.70	1.77	1.84	1.87	1.91	1.92	1.91	1.90	1.86	1.86	1.83
	293	2.67	2.49	2.44	2.41	2.38	2.30	-0.23	-0.23	-0.22	-0.18	-0.15	-0.10	-0.04	0.07	0.18	0.28	0.37	0.50	0.62	0.73	0.81	0.92	1.04	1.13	1.17	1.21	1.25	1.30	1.35	1.34	1.33	1.30	1.29	1.27
	292	3.84	3.63	3.59	3.56	3.54	3.46	-0.74	-0.75	-0.76	-0.76	-0.75	-0.71	-0.67	-0.60	-0.52	-0.45	-0.35	-0.25	-0.15	00.0	0.15	0.25	0.36	09.0	0.77	0.95	1.10	1.25	1.35	1.35	1.34	1.31	1.30	1.27
cations	Elevation	0.56					-	0.57	0.58	0.60	0.61	0.62	0.64	0.65	0.67	0.68	69.0	0.71	0.72	_					•						-				-
Piezometer Locations	Station	15.00U	8.79	6.750	4.790	2.79U	1.790	0.080	0.22D	0.36D	0.500	0.64D	0.780	0.92D	1.06D	1.20D	1.340	1.48D	1.62D	1.76D	1.90D	2.04D	2.18D	2.46D	2.74D	3.02D	3.30D	3.58D	3.86D	4.80D	00 7. 9	8.04D	009.6	11.150	12.70D
Pie	No.	4	5	9	7	∞	6	14	15	91	17	18	19	20	2.1	2.2	23	24	25	26	27	28	59	30	31	32	33	34	35	36	37	38	39	70	41

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- 1	Piezometer Locations	ocations						۔ا	Number*					
8	Station	Elevation	335	336	337	338	339	340	341	342	343	344	345	346
4	15.00U	0.56	5.60	5.33	4.74	3.44	4.10	4.66	5.39	3.45	4.02	4.61	4.45	3.55
'n	8.79U		5.59	5.31	4.72	3.41	4.07	4.63	5.34	3.39	3.96	4.55	4.37	3.45
9	6.75U		5.58	5.31	4.72	3.40	4.06	4.62	5.33	3.37	3.95	4.53	4.34	3.41
7	4.79U		5.57	5.31	4.72	3.40	4.06	4.62	5.32	3.37	3.94	4.52	4.33	3.41
æ	2.790		5.57	5.31	4.72	3,39	4.05	4.62	5.32	3.36	3.94	4.52	4.32	3.40
6	1.790		5.57	5.30	4.71	3.38	4.04	4.60	5.30	3.34	3.91	4.50	4.30	3.36
14	0.080		1.65	1.30	0.76	0.59	1.20	1.92	0.90	0.27	0.95	1.50	-0.05	-0.17
15	0.22D		1.64	1.29	0.75	0.58	1.19	1.92	0.89	0.26	0.94	1.49	-0.06	-0.18
16	0.36D		1.63	1.28	0.74	0.57	1.18	1.91	0.88	0.25	0.93	1.48	-0.07	-0.19
17	0.50D	-	1.63	1.27	0.74	0.57	1.17	1.91	0.87	0.25	0.92	1.48	-0.08	-0.19
18	0.64D	0.57	1.63	1.27	0.74	0.57	1.16	1.91	0.87	0.24	0.92	1.48	-0.08	-0.18
19	0.780	0.58	1.64	1.28	0.74	0.57	1.17	1.91	0.87	0.24	0.93	1.49	-0.07	-0.17
20	0.92D	0.59	1.65	1.29	0.75	0.57	1.18	1.91	0.87	0.25	0.94	1.50	-0.06	-0.14
21	1.06D	0.61	1.66	1.31	0.76	0.58	1.19	1.91	0.88	0.26	0.95	1.52	-0.05	-0.12
22	1.20D	0.62	1.67	1.33	0.77	0.59	1.20	1.92	0.89	0.28	0.97	1.55	-0.03	-0.09
23	1.340	0.64	1.68	1.34	0.78	0.61	1.21	1.92	0.91	0.30	1.00	1.57	-0.01	-0.05
24	1.48D	0.65	1.70	1.35	0.79	0.64	1.23	1.93	0.94	0.35	1.04	1.60	0.03	0.01
25	1.62D	19.0	1.72	1.36	0.80	0.66	1.25	1.95	0.97	0.40	1.08	1.65	0.07	0.10
56	1.76D	0.68	1.75	1.37	0.82	0.68	1.27	1.98	1.01	0.44	1.11	1.70	0.12	0.19
27	1.900	0.69	1.77	₹.39	0.84	0.70	1.28	2.00	1.03	0.47	1.14	1.74	0.18	0.27
28	2.04D	0.71	1.79	1.40	0.86	0.73	1.30	2.02	1.07	0.51	1.17	1.78	0.24	0.32
29	2.18D	0.72	1.81	1.42	0.88	0.75	1.32	2.05	1.09	0.55	1.21	1.85	0.28	0.38
31	2.46D	0.75	1.87	1.50	0.93	0.80	1.36	2.12	1.14	0.62	1.28	1.95	0.42	0.50
33	2.74D	0.78	1.92	1.60	0.99	0.85	1.40	2.16	1.23	0.70	1.36	2.04	0.55	0.61
34	3.02D	08.0	1.96	1.65	1.05	0.88	1.45	2.20	1.28	0.77	1.43	2.08	0.65	0.71
35	3.30D	0.83	2.00	1.71	1.12	0.92	1.49	2.25	1.37	0.83	1.50	2.15	0.75	0.83
36	3.580	0.86	2.04	1.76	1.16	0.95	1.60	2,30	1.45	06.0	1.60	2.20	0.87	0.94
37	3.86D	0.88	2.10	1.79	1.20	1.00	1.68	2.34	1.53	1.00	1.69	2.26	0.98	1.05
39	4.42D		2.20	1.85	1.30	1.10	1.78	2.43	1.72	1.17	1.80	2.37	1.17	1.20
41	6.96D		2.22	1.88	1.34	1.22	1.82	2.50	1.87	1.21	1.86	2.43	1.25	1.25
42	8.040		2.22	1.88	1.34	1.21	1.82	2.50	1.87	1.21	1.86	2.43	1.25	1.24
43	09.6		2.22	1.88	1.34	1.21	1.82	2.50	1.86	1.20	1.85	2.42	1.25	1.24
77	11.150		2.22	1.88	1.34	1.21	1.82	2.50	1.86	1.20	1.85	2.41	1.25	1.24
45	12.70D	-	2.26	1.88	1.34	1.20	1.80	2.49	1.86	1.19	1.84	2.41	1.25	1.23
						o)	(Continued)							
							,							

Average Piezometer Readings, Type 5 Expansion

Table 6

* Refer to Table 1 for flow conditions for each run.

(Sheet 1 of 3)

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Table 6 (Continued)

	359	2.52	2.32	2.26	2.23	2.21	2.10	-0.70	-0.70	-0.66	-0.63	-0.54	-0.41	-0.30	-0.15	0.00	0.12	0.22	0.35	0.45	0.54	79.0	0.72	0.87	0.98	1.05	1.12	1.20	1.24	1.31	1.33	1.31	1.30	1.29	1.28
	358	3.60	3.38	3.32	3.30	3.28	3.19	0.65	0.65	0.67	0.73	0.82	0.95	1.09	1.15	1.30	i.41	1.55	1.65	1.72	1.80	1.90	1.97	5.06	2.15	2.19	2.23	2.30	2.36	2.45	2.51	2.50	2.49	2.48	2.46
	357	2.98	2.80	2.72	5.69	2.67	7.60	0.02	0.01	0.04	0.07	0.17	0.30	0.42	0.54	19.0	0.80	0.89	1.00	1.11	1.19	1.26	1.34	1.44	1.52	1.60	1.68	1.72	1.77	1.84	1.88	1.86	1.85	1.84	1.83
	356	2.35	2.15	2.10	2.07	2.05	1.96	-0.54	-0.55	-0.51	-0.45	-0.34	-0.23	-0.12	00.0	0.12	0.25	0.36	0.47	0.55	79.0	0.69	0.77	0.85	0.95	1.00	1.08	1.15	1.19	1.27	1.29	1.27	1.26	1.25	1.24
	355	3.56	3.35	3.30	3.27	3.25	3.16	-1.00	-1.01	-1.02	-1.00	-0.98	-0.92	-0.85	-0.76	-0.64	-0.50	-0.32	-0.15	0.00	0.10	0.24	0.35	0.52	0.68	0.75	0.86	0.98	1.06	1.22	1.27	1.26	1.25	1.24	1.23
	354	3.43	3.23	3.19	3.18	3.16	3.09	-0.73	-0.74	-0.75	-0.76	-0.75	-0.70	-0.65	-0.54	-0.35	-0.20	-0.08	0.05	0.15	0.22	0.35	0.45	0.57	0.75	98.0	96.0	1.08	1.15	1.25	1.34	1.33	1.32	1.31	1.30
1 -	353	4.22	4.06	4.03	4.00	3.98	3.92	0.87	0.86	0.85	0.85	0.88	0.93	0.97	1.05	1.17	1.31	1.39	1.48	1.57	1.65	1.73	1.80	1.92	2.08	2.15	2.24	2.33	2.40	2.50	2.52	2.51	2.50	2.49	2.48
Run	352	3.66	3.50	3.45	3.43	3.42	3.35	0.20	0.19	0.18	0.18	0.20	0.26	0.35	0.44	0.53	0.65	0.75	0.85	0.95	1.07	1.15	1.24	1.40	1.55	1.60	1.70	1.78	1.84	1.92	1.92	1.91	1.90	1.89	1.88
	351	2.96	2.80	2.76	2.75	2.74	2.69	-0.42	-0.43	-0.43	-0.43	-0.42	-0.38	-0.30	-0.20	-0.11	00.00	0.10	0.22	0.35	0.41	0.50	0.60	0.73	0.85	0.00	0.98	1.06	1.15	1.25	1.27	1.26	1.25	1.24	1.23
	350	4.04	3.91	3.88	3.87	3.86	3.80	-0.45	-0.46	-0.47	-0.47	-0.45	-0.42	-0.38	-0.32	-0.28	-0.21	-0.15	-0.07	0.01	0.08	0.14	0.22	0.40	0.57	0.70	0.83	0.95	1.06	1.22	1,28	1,27	1.27	1.26	1.25
	349	3.09	3.00	2.98	2.97	2.96	2.93	0.08	0.07	90.0	90.0	0.07	0.08	0.10	0.13	0.18	0.24	0.30	0.35	0.45	0.52	0.57	0.62	0.73	0.85	0.00	0.95	1.00	1.07	1.22	1.26	1.25	1.25	1.24	1.24
	348	4.72	4.62	4.58	4.57	4.56	4.53	0.98	0.97	96.0	96.0	0.97	0.98	1.02	1.07	1.09	1.13	1.20	1.30	1.38	1.48	1.57	1.67	1.80	1.90	1.97	2.08	2.21	2.30	2.40	2.42	2.41	2.40	2.40	2.39
	347	4.20	4.09	4.06	4.05	4.03	3.99	0.47	0.46	0.45	0.44	0.44	0.45	0.48	0.52	0.58	0.63	0.70	0.80	0.90	0.97	1.02	1.07	1.15	1.32	1.40	1.51	1.62	1.68	1.84	1.91	1.90	1.90	1.89	1.88
Locations	Elevation	0.56	_		_					•	-	0.57	0.58	0.59	0.61	0.62	0.64	0.65	0.67	0.68	69.0	0.71	0.72	0.75	0.78	08.0	0.83	0.86	0.88				_		-
Piezometer L	Station	15.00U	8.790	6.75U	4.79U	2.79U	1.790	0.080	0.22D	0.36D	0.500	0.640	0.780	0.920	1.06D	1.20D	1.34D	1.48D	1.62D	1.76D	1.900	2.04D	2.180	2.46D	2.74D	3.02D	3.30D	3.58D	3.86D	4.42D	6.96D	8.040	9.60D	11.15D	12.70D
Pi	No.	7	S	9	7	œ	6	14	15	16	17	18	19	20	21	22	23	54	25	56	27	28	53	31	33	34	35	36	37	39	41	77	۶،	7',	4.5

Table 6 (Concluded)

	371	1.92	1.62	1.52	1.48	1.45	1.31	1.09	1.12	1.09	1.07	1.15	1.24	1.31	1.36	1.42	1.46	1.51	1.55	1.59	1.62	1.65	1.68	1.75	1.82	1.86	1.90	1.95	1.99	1.99	1.99	1.97	1.96	1.95	7,6
	370	1.92	1.67	1.59	1.55	1.53	1.41	1.24	1.26	1.23	1.22	1.29	1.39	1.43	1.47	1.53	1.56	1.60	1.63	1.66	1.69	1.72	1.75	1.81	1.86	1.90	1.94	1.98	2.01	2.00	2.00	1.98	1.97	1.96	1 95
	369	2.50	2.20	2.15	2.11	2.08	1.94	1.80	1.82	1.80	1.78	1.85	1.93	1.98	2.02	2.08	2.12	2.15	2.18	2.22	2.25	2.28	2.30	2.35	2.39	2.43	2.47	2.50	2.53	2.52	2.52	2.51	2.50	2.48	97 6
	368	2.06	1.77	1.69	1.65	1.62	1.47	0.35	0.62	0.85	1.05	1.15	1.22	1.29	1.34	1.39	1.44	1.48	1.52	1.55	1.59	1.63	1.66	1.72	1.77	1.83	1.87	1.92	1.95	1.95	1.96	1.93	1.92	1.90	1 88
	367	2.01	1.76	1.68	1.65	1.63	1.52	0.51	0.72	0.98	1.11	1.20	1.28	1.33	1.38	1.42	1.45	1.50	1.55	1.58	1.61	1.64	1.67	1.73	1.78	1.83	1.87	1.91	1.94	1.93	1.93	1.91	1.90	1.88	1 86
	366	2.63	2.40	2.33	2.30	2.27	2.15	1.15	1.36	1.63	1.77	1.89	1.94	1.99	2.04	2.08	2.12	2.16	2.20	2.23	2.26	2.28	2.31	2.35	2.39	2.43	2.48	2.52	!	;	1	;	!	2.51	2 50
D	365	2.06	1.74	1.64	1.61	1.58	1,41	-1.00	-1.02	-0.92	-0.75	-0.53	-0.25	-0.08	0.10	0.22	0.35	0.47	0.57	0.65	0.70	0.75	0.80	0.94	1.03	1.10	1.15	1.22	1.30	1.36	1.40	1.37	1.35	1.33	1 21
	364	1,75	1.53	1.46	1.42	1.41	1.30	-0.50	-0.52	-0.45	-0.35	-0.15	0.02	0.15	0.30	0.43	0.53	0.62	0.67	0.74	0.81	0.85	0.89	0.98	1.04	1.08	1.12	1.17	1.21	1.23	1.25	1.23	1.22	1.20	1 10
	363	3,03	2.79	2.72	2.69	2.67	2.60	1.00	0.98	1.02	1.16	1.32	1.48	1.60	1.70	1.82	1.93	2.00	2.05	2.10	2.15	2.18	2.22	2.27	2.34	2.40	2.44	2.46	2.49	2.52	2.53	2.52	2.51	2.50	07 6
	362	2.40	2.19	2.12	2.09	2.05	1.96	0.32	0.31	0.37	0.43	0.71	0.84	0.97	1.10	1.20	1.28	1.34	1.41	1.47	1.52	1.56	1.61	1.67	1.73	1.76	1.79	1.82	1.85	1.88	1.92	1.91	1.90	1.88	1.87
	361	1.79	1.55	1.49	1.46	1.44	1.35	-0.25	-0.26	-0.20	-0.05	0.08	0.22	0.37	0.47	0.58	0.69	0.76	0.82	0.00	0.95	0.97	1.02	1.09	1.15	1.20	1.24	1.28	1.31	1.32	1.32	1.30	1.29	1.28	1, 27
	360	2.69	2.44	2.37	2.34	2.32	2.20	-1.05	-1.05	-1.00	-0.95	-0.84	-0.68	-0.55	-0.40	-0.18		0.05	0.17	0.28	0.40	0.50	0.59	0.72	0.85	0.92	1.00	1.10	1.19	1.28		1.29	1.27	1.26	1.25
900	Elevation	0.56	_			_			_	-•	-	0.57	0.58	0.59	0.61	0.62	0.64	0.65	0.67	0.68	69.0	0.71	0.72	0.75	0.78	0.80	0.83	98.0	0.88	_					-
Diomomorphism Constitution	Station	15.00U	8.79U	6.75U	4.79U	2.790	1.790	0.08D	0.22D	0.36D	0.500	0.64D	0.780	0.92D	1.06D	1.20D	1.34D	1.48D	1.62D	1.76D	1.900	2.04D	2.18D	2.46D	2.74D	3.02D	3.30D	3.58D	3.5oD	4.42D	6.96D	8.040	9.60D	11.150	12,70b
90	%	4	Ŋ	9	7	œ	6	14	15	16	17	18	19	20	21	22	23	54	25	26	27	28	53	31	33	34	35	36	37	39	41	42	43	77	57

Table 7

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Average Piezometer Readings, Type 6 Expansion

1d	Piezometer Locations	ocations								Run Numbe	* 10						
No.	Station	Elevation	372	373	374	375	376	317	378	379	380	381	397	398	399	382	383
4	15.000	0.56	3.36	3.77	4.92	4.55	3.75	4.67	2.45	3.81	2.84	3.93	4.07	3.58	2.96	3.26	£.
5	8.79	_	3.33	3.74	4.88	4.51	3.70	7.60	2.42	3.70	2.75	3.90	3.89	3.45	3.85	3.13	3.34
ا ع	6.750		3.33	3.73	4.87	4.50	3.68	4.58	2.41	3.67	2.73	3.89	3.85	3.41	2.82	3.09	3.19
- 0	06/.4	_	3.32	3.73	78.4	67.7	3.67	4.57	2.41	3.65	2.72	3.87	3.82	3.40	2.81	3.07	3.17
00	767.1		3.32	3.72	98.4	4.49	3.66	4.56	2.40	3.66	2.71	3.86	3.80	3.38	2.80	3.05	3.15
^ 2	080		35.01	3.71	4.00	7.0	7.0	4.0	2.39	3.61	2.68	3.81	3.73	3.32	2.76	86.	3.06
15	0.220	-	24.0	1.03	0.75	0.00		77.0	0.63	0.14	-0.17	-0.21	20.55	-0.33	-0.10)) (-1.15
16	0.36D		0.33	1.01	0.73	0.86	53	0.22	190	100	27.0-	27.0-	20.01	10.33	10.0	71.0-	7
17	0.50D		0.32	1.00	0.72	0.85	0.52	0.21	0.61	60.0	-0.23	-0.24	-0.58	-0.36	-0-13	-0.13	11.17
18	0.64D	_	0.31	0.99	0.71	0.84	0.51	0.20	0.61	0.08	-0.22	-0.24	-0.50	-0.35	-0.13	-0.10	
19	0.78D		0.32	66.0	0.72	0.83	0.51	0.21	0.61	60.0	-0.20	-0.24	-0.42	-0.30	-0.10	-0.05	-1.10
50	0.920		0.33	1.00	0.74	0.85	0.52	0.23	0.63	0.13	-0.16	-0.21	-0.26	-0.23	-0.04	0.04	-0.96
7 5	1.06D		0,35	1.01	0.76	0.89	0.55	0.27	0.65	0.19	-0.10	-0.10	-0.12	-0.11	0.0	0.14	-0.78
7.7	1.20D		0.37	1.03	0.78	0.92	09.0	0.33	0.67	0.27	-0.02	0.01	0.08	00.0	0.19	0.27	-0.60
7 7	1.340	-	0.40	1.05	0.83	0.95	0.65	0.39	0.72	0.37	0.05	0.13	0.28	0.16	0.32	0.45	-0.35
5 7	1.480	-•	0.45	1.07	0.86	1.00	0.71	0.50	0.76	0.50	0.15	0.28	05.0	0.36	0.45	0.66	-0.15
77	1.020	- :	0.50	1.10	0.91	1.04	0.80	0.60	0.80	0.65	0.24	0.42	0.70	0.53	0.55	0.83	0.02
27	1.760	75.0	0.55	1,14	76.0	1.07	0.86	0.71	0.85	0.75	0.35	0.58	0.82	0.62	0.66	0.92	0.14
7 %	2 040	0.58	65.0	1.19	1.01	1.12	0.93	0.87	0.89	0.85	0.42	0.66	0.95	0.73	0.77	1.03	0.25
30	2 190	8.4	70.0	7.24	1,09	1.21	3.5	0.92	0.94	86.0	0.50	0.77	1.05	0.85	0.88	1.15	0.42
3 6	2.320	0.61	0.0	1.29	1.10	1,27	97:	1.00	86.0	1.06	0.60	0.85	1.12	0.95	0.95	1.21	0.55
3 2	2.460	79.0	0.75	1.35	1.22	1.33	1.12	1.07	1.07	1.12	79.0	0.94	1.22	1.03	1.00	1.30	0.63
32	2.600	65.0	80	0, 1	1.27	1,36	1.1/	1.12	60.1	1.20	0.73	1.05	1.28	1.10	1.05	1.36	0.70
33	2.74D	0.67	0.84	1.45	200	1.42	1.25	1.20	1.00	1.30	79.0	1.14	1.35	1.16	1.10	1.4.	9.7
34	2.88D	0.68	0.89	1.49	1,44	1.48	1.35	1.38	1.15	1.45	66.0	1.20	1.40	1.42	1.13	7.5	0.0
35	3.02D	0.69	0.93	1.53	1,51	1,51	1.40	1.45	1.17	1.52	0.97	77	5.5	1.32	7, 1	1	
36	3.160	0.71	96.0	1.56	1.57	1.56	1.45	1.51	1.19	1.57	1.00	1.40	1.55	1.36	1.27		7 0
37	3.300	0.72	0.99	1.60	1.62	1.61	1.50	1.56	1.20	1.63	1.04	1.47	1.60	1.43	1.32	1.65	1.15
2 5	3.440	0.74	1.02	1.63	1.66	1,65	1,55	1.59	1.21	1.67	1.06	1.52	1.65	1.46	1.35	1.69	1.18
Ž ć	3.380	0.75	50.	1.66	1.70	1.69	1.57	1.62	1.23	1.70	1.08	1.57	1.71	1.52	1.38	1.72	1.25
3 7	3 860	0.70	7.0	1.08	1.74	1.73	1.60	1.6/	1.24	1.72		1.63	1.74	1.55	1.41	1.75	1.29
4.7	4.140	07.0	1.03	1.70	1.11	1.73	1.63	7.7	1.25	1./2 ::	1.14	1.66	1.77	1.64	1.44	1.77	1.34
7 5	4.420	0.83	1.12	1.72	1.01	1.70	1.65	1,70	1.20	7.7	97.7	1.69	1.81	1.68	1.47	1.79	1.37
77	4.700	0.86	71.1	77.	20.1	1.01	1.07	0,11	1.27	1./9		1.7	1.85	1.72	1.50	1.87	1.42
45	4.98D	0.88	1.15	1 75	98.1	1 85	1.00	1.00	1.20	1.02	1.21		99.1	9, ,	1.53	1.84	1.48
97	5.260	} -	1.15	75	20.1			1,02	1.29		77.1	1.//	06.1	\	1.54	1.86	1.50
47	5.540		1.15	1.74	96.	1.85	0/.1	2,07	67.1	78.1 78.1	1.22	1.11	1.90	1.77	1.54	1.87	2:5
87	6.480		1.15	1 74	285	280	2.5	2,0	1 20	100	1.66	\ . · ·	1.90	7.7.	1.54	/8.1	1.51
67	8.04D		1.15	1.73	1.85	1.85	2 2 7	1.84	1.29	1.04	1.21	1.70	1.88	1.76	1.53	1.67	1.49
20	9.600		1.15	1.73	1.85	1.85	1.70	78.	1.28	1.82	1.19	1 76	, o	7.7	1.74	70.1	01.
51	11.150		1.15	1.73	1.84	1.85	1,70	1,83	1.28	1.82	1.18	1.73	1.85	1.72	1.01	. 8	1.4
52	12.70D	-	1,15	1.73	1.84	1.85	1.70	1,83	1.28	1.81	1 18	1.73	1.85	1.71	1.48	1.82	1.45
								(Cont	(Continued)								
									,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,								

* Refer to Table 1 for flow conditions for each run.

۵.	Precometer Lecations	Suettee	:						Kun	Number							
1	Station	Flevation	É	92	107	20,	385	386	387	388	389	390	391	392	393	394	395
٠	1000.01	97.10	2.6.	7.45	2.03	2.42	2.78	2.95	2.59	2.16	2.46	2.40	2.22	2.46	2.55	2.40	2.24
^	x		96.5	17.5	-1	2,25	2.57	2.68	2.44	1.94	2.15	2.14	1.96	2.19	2.31	2.11	1.90
ç	1000		1	3.15	2.60	7.30	2.52	2.62	2.40	1.88	2.08	2.08	1.89	2.11	2.25	2.05	1.80
	¥	_	2.4b	3.12	7.64	2.18	2.51	2.58	2.37	1.85	2.03	2.04	1.85	2.07	2.21	2.00	1.75
i,	ž		7.7	3.10	2.62	2.16	2.49	2.56	2,35	1.83	2.01	2.01	1.82	5.04	2.19	1.97	1.72
	F		. 38	56.	₹.	2.10	2.40	2.45	2.29	1.73	1.87	1.90	1.70	1.90	5.08	1.84	1.55
			-0.31	-0.70	-0.65	-0.57	-0.17	-0.81	0,40	90.0	-0.20	0.03	17.0	0.78	1.17	1.70	1.39
	9.5		-0.32	-0.71	-0.66	-0.58	-0.18	-0.82	0.39	90.0	-0.22	0.01	96.0	1.07	1.41	1.73	1.43
•	11. 35,0		-0.33	-0.70	-0.66	-0.58	-0.16	-0.79	0.40	0.12	-0.15	0.08	1.18	1.36	1.61	1.75	1.45
	11. 305.		-0.33	-0.65	-0.61	-0.57	-0.12	-0.71	0.44	0.30	0.03	0.28	1.32	1.53	1.75	1.77	1.47
x.	372.0		-0.30	-0. h0	70.25	-0.54	-0.04	-0.61	0.50	0.43	0.25	0.50	1.37	1.60	1.80	1.75	1.44
÷	1,00		-0.25	-0.47	-0.42	-0.44	0.10	-0.40	0.63	0.30	0.50	0.62	1,41	1.61	1.81	1.73	1.42
27	6.425		-0.16	-0.29	~0.26	-0.33	0.30	-0.15	0.75	0.85	0.75	0.88	1.42	1.62	1.82	1.72	1.41
7.3	1.000	_	-0.08	-0.03	-0.05	-0.20	0.51	0.05	0.92	0.95	0.92	1.07	1.42	1.63	1.83	1.72	1.42
-1	1.200		0.05	07.50	0.15	0.00	0.70	0.32	1.04	1.05	96.0	1.16	1.42	1.63	1.79	1.69	1.38
2.5	i. 84D		0.15	07.0	0.31	0.20	0.88	0.50	1.15	1.08	1.06	1.21	1.42	1.62	1.81	1.70	1.39
•	1.465	~•	o. 10	0.58	0.45	0.35	1.03	0.65	1,25	1.11	1.08	1.23	1.40	1.58	1.79	1.66	1.35
ń	1.5.1	-	0.47	0.75	0,00	0.48	1.10	0.79	1.35	1.12	1.12	1.25	1.39	1.56	1.78	1.64	1.32
ž,	1.750	6.57	09.0	0.91	0.72	09.0	1.17	0.90	1.40	1.14	1.14	1.27	1.42	1.59	1.80	1.67	1.37
h	1.400		0.68	1.05	0.82	0.68	1.25	1.02	1.45	1.22	1.22	1.35	1.52	1.70	1.90	1.79	1.51
£	2.0+0	0.60	0.77	1.15	0.92	0.75	1.31	1.12	1.50	1.27	1.30	1.4]	1.57	1.77	1.95	1.85	1.59
Ī,	1.180	0.51	0.86	1.25	1.01	0.80	1.35	1.17	1.55	1.31	1.35	1.46	1.62	1.82	1.99	1.90	1.63
50	2.320	0.65	0.91	1.33	1.08	0.85	1.39	1.23	1.59	1.36	1.40	1.52	1.67	1.87	2.02	1.95	1.69
::	7.46D	9.64	0.94	1.40	1.11	0.00	1.44	1.26	1.62	1.39	1.45	1.45	1.69	1.90	5.04	1.98	1.72
77	2.600	0.65	0.98	1.47	1.16	76.0	1.48	1.30	1.65	1.43	1.50	1.59	1.72	1.95	2.08	2.02	1.77
	2.740	0.67	1.03	1.52	1.20	0.98	1.51	1.35	1.68	1.45	1.55	1.63	1.74	1.98	2.11	2.04	1.80
1	1,48D	0.58	1.05	1.55	1.24	1.02	1.55	1.41	1,71	1.48	1.59	1.65	1.77	2.01	2.14	2.07	1.85
2	3.020	69.0	1.10	1.59	1.29	1.06	1.58	1.47	1.74	1.51	1.63	1.70	1.79	2.04	2.17	2.10	1.88
36	3.160	0.71	1.1	1.62	1.33	1.10	1.61	1.50	1.76	1.54	1.66	1.73	1.82	2.07	2.19	2.12	1.91
3.7	3.30E	0.72	1.18	1.65	1.36	1.12	1.64	1.54	1.78	1.56	1.69	1.75	1,85	2.09	2.21	2.15	1.95
S	3.440	57.0	1.21	1.69	1.39	1.14	1.66	1.58	1.80	1.58	1.72	1.77	1.88	2.13	2.23	2.18	1.98
<u>.</u>	3.580	0.75	1.23	1.74	1.42	1.16	1.69	1.61	1.82	1.61	1.74	1.80	1.91	2.16	2.25	2.20	2.01
o+	3.7.10	0.76	I. 26	1.78	7.4.	1.18	1.73	1.66	1.85	1.63	1.77	1.83	1.93	2.19	2.27	2.23	2.04
7	3.860	0.78	1.29		1.48	1.21	1.76	1.69	1.87	1.66	1.80	1.86	1.96	2.22	2.29	2.25	2.07
7	4.140	6.81	= :	1.86	1.53	1.24	1.80	1.74	1.90	1.70	1.86	1.90	2.00	2.26	2.33	2.29	2.11
~ , †	(17.4.7)	0.83	1.34	1.90	1.57	128	1.85	1.78	1.93	1.74	1.91	1.94	2.04	2.30	2.37	2.33	2.16
ਪੂਰ ਪ੍ਰ	4.700	0,8h	1.38	1.94	1.62	1.32	1.89	1.82	1.94	1.77	1.96	1.98	2.08	2.35	2.40	2.37	2.21
19	4.980	0.84	1.39	1.97	1.66	1.36	1.92	1.85	1.95	1.80	5.00	2.01	2.12	2.38	2.44	2.41	2.24
· +	5.26D		1.39	1.98	1.67	1.36	1.92	1.86	1.95	1.79	1.99	2.01	2.11	2.37	2.43	2.40	2.23
1.5	5.540		1.39	1.99	1.67	1.35	1.92	1.86	1.95	1.79	1.99	5.00	2.10	2.37	2.43	2.40	2.23
00 -1	4.480	_	1.18	3.09	1.65	7.	1,92	1.86	1.95	1.79	1.99	.00	2.10	2.37	2.43	2.40	2.23
5.7	8.040			1.98	1.65	. <u></u>	1.90	1.84	1.94	1.78	1.97	1.49	5.09	2.35	2.41	2.38	2.22
90	9.600		1.37	1.97	<i>i</i> .	1.32	1.88	1.82	1.92	1.77	1.96	1.98	5.08	2.34	2.40	2.37	2.21
Τ.	11.155		1.57	1.95	1.62	1.31	1.87	1.80	2.	1.76	1.94	1.96	5.06	2.32	2.39	2.36	2.20
Ç.	12,705	-	÷.	<u>;</u>	1.40	1.29	. 8 6	1.78	06.1	. 75	. 9.	· ·	7.04	2.30	2.37	2.34	2.17

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Table 8 Average Piezometer Readings, Type 7 Expansion

۵	Piezometer Locations	Locations								Run	imber*						
No.	Station	Elevation	430	431	432	427	428	429	424	425	426	421	422	433	418	419	420
4	15.00U	0.56	4.92	4.28	3.77	4.36	3.23	2.37	3.85	3.55	2.76	3.86	3.41	2.87	3.58	3.18	2.68
5	8.790	_	4.88	4.23	3.74	4.27	3.17	2,35	3.70	3.43	2.67	3.66	3.25	2.74	3.35	3.01	2.52
9	6.75U	_	4.87	4.22	3.74	4.25	3.16	2.33	3.68	3.41	2.63	3.62	3.21	2.71	3.30	2.98	2.49
7	4.79U		4.86	4.21	3.73	4.24	3.15	2.33	3.66	3.39	2.62	3.59	3.19	2.69	3.26	2.96	2.47
80	2.79U		4.85	4.21	3.72	4.22	3.14	2.32	3.64	3.38	2.61	3.57	3.17	2.67	3.23	2.94	2.45
6	1.790		4.83	4.20	3.71	4.20	3.12	2.30	3.59	3.33	2.58	3.52	3.10	2.62	3.14	2.87	2.39
14	0.080		0.35	0.62	0.86	-0.07	0.21	0.39	-0.37	0.00	-0.15	-0.65	-0.40	-0.12	-1.10	-0.25	-0.27
15	0.220		0.33	09.0	0.85	-0.09	0.19	0.38	-0.41	-0.02	-0.17	-0.67	-0.43	-0.14	-1.15	-0.27	-0.30
16	0.36D		0.31	0.58	0.84	-0.10	0.18	0.37	-0.44	-0.02	-0.19	-0.68	-0.45	-0.17	-1.19	-0.26	-0.28
17	0.500		0.30	0.57	0.83	-0.11	0.17	0.35	-0.47	-0.01	-0.21	-0.66	-0.42	-0.16	-1.17	-0.22	-0.26
18	0.64D		0.29	0.58	0.82	-0.08	0.16	0.34	-0.44	0.01	-0.19	-0.62	-0.38	-0.13	-1.12	-0.18	-0.22
19	0.780		0.33	0.59	0.83	-0.07	0.18	0.35	-0.39	0.03	-0.17	-0.58	-0.34	-0.09	-1.00	-0.12	-0.17
20	0.92D		0.34	0.61	0.84	-0.04	0.21	0.36	-0.32	90.0	-0.14	-0.46	-0.28	-0.03	-0.86	0.04	-0.06
21	1.06	-	0.38	0.64	0.87	0.02	0.27	0.41	-0.20	0.19	-0.08	-0.34	-0.12	0.0	-0.65	0.17	0.02
22	1.20D		0.40	0.68	0.89	0.10	0.32	0.43	-0.10	0.31	-0.02	-0.14	0.03	0.23	-0.38	0.36	0.18
23	1.34D		0.43	0.73	0.93	0.21	0.37	0.44	-0.03	0.41	0.04	90.0	0.11	0.36	-0.22	0.55	0.34
77	1.48D		65.0	0.81	96.0	0.31	0.43	0.48	0.12	0.56	0.15	0.28	0.31	67.0	0.04	0.71	97.0
25	1.62D		0.57	0.86	1.01	0,40	0.51	0.52	0.41	0.74	0.37	0.44	0.47	0.63	0.28	0.87	0.58
56	1.76D		0.61	0.91	1.06	0.52	0.58	0.58	99.0	0.85	0.45	0.56	0.67	0.77	0.48	0.99	0.72
27	1.90D		0.68	0.97	1.11	0.61	99.0	0.63	0.79	0.98	0.53	0.73	0.78	0.87	99.0	1.13	0.84
28	2.04D		0.80	1.07	1.19	0.82	0.75	0.68	0.87	1.08	0.62	0.84	0.94	0.93	0.78	1.17	0.90
53	2.18D		0.87	1.12	1.23	0.91	0.81	0.74	0.98	1.18	0.68	1.03	1.07	1.00	06.0	1.28	0.97
30	2.45D	_	1.11	1.26	1.36	1.12	0.95	0.87	1.21	1.37	1.83	1.19	1.19	1.12	1.04	1.37	1.07
31	2.73D		1.33	1.33	1.51	1.28	1.12	0.97	1.31	1.48	0.97	1.26	1.26	1.21	1.14	1.39	1.12
32	3.010	-•	1.48	1.47	1.63	1.40	1.22	1.04	1.42	1.56	1.03	1.38	}	1.25	1.21	1.43	1.16
33	3 29D	•	1.58	1.33	1.67	1.50	1.28	1.08	1.47	1.58	1.08	1.41	1.35	1.31	1.24	1.45	1.18
35	3.710	0.57	1.67	1.64	1.69	1.54	1.33	1,10	1.48	1.59	1.11	1.43	1.37	1.30	1.22	1.47	1.19
38	4.130	0.61	1.72	1.70	1.73	1.61	1.36	1.13	1.57	1.66	1.17	1.52	1.48	1.38	1.36	1.58	1.23
17	4.55D	0.65	1.74	1.73	1.74	1.64	1.39	1.15	1.62	1.71	1.21	1.59	1.55	1.43	1.48	1.64	1.30
77	4.97D	69.0	1.76	1.74	1.75	1.67	1.41	1.17	1.66	1.75	1.24	1.65	1.61	1.47	1.57	1.70	1.35
41	5.39D	0.74	1.77	1.75	1.76	1.69	1.43	1.18	1.70	1.17	1.27	1.69	1.67	1.50	1.63	1.74	1.39
20	5.810	0.78	1.78	1.76	1.77	1.71	1.44	1.20	1.73	1.79	1.29	1.73	1.70	1.53	1.67	1.77	1.42
21	6.09D	0.81	1.79	1.76	1.77	1.72	1.45	1.20	1.75	1.81	1.30	1.76	1.73	1.55	1.71	1.80	1.45
25	6.37D	0.83	1.79	1.77	1.78	1.73	1.46	1.21	1.77	1.84	1.31	1.79	1.76	1.57	1.74	1.82	1.47
53	6.65D	0.86	1.79	1.77	1.78	1.74	1.47	1.21	1.79	1.86	1.32	1.82	1.78	1.58	1.78	1.85	1.49
24	8.02D	0.88	1.79	1.77	1.78	1.74	1.47	1.20	1.78	1.85	1.32	1.81	1.77	1.59	1.76	1.84	1.48
55	9.57D	0.88	1.79	1.77	1.78	1.74	1.46	1.20	1.77	1.84	1.31	1.80	1.77	1.58	1.75	1.83	1.47
99	11.120	0.88	1.79	1.77	1.78	1.73	1.45	1.20	1.76	1.83	1.30	1.79	1.76	1.57	1.74	1.82	1.46
27	12.67D	0.88	1.78	1.76	1.76	1.72	1.44	1.20	1.75	1.82	1.29	1.76	1.75	1.56	1.72	1.81	1.36
								ٽ	Continued	<u></u>							

* Refer to Table 1 for flow conditions for each run.

Table 8 (Concluded)

	405	2.10	1.78	1.68	1.64	1.61	1.45	1.28	1.32	1.33	1.33	1.33	1.32	1.31	1.31	1.33	1.30	1.30	1.29	1.29	1.28	1.27	1.27	1.26	1.24	1.23	1.21	!	ł	1	ł	ł	!	1.92	1.97	2.02	2.03	2.03	2.02	2,00
	404	2.48	2.18	2.11	2.09	2.05	1.92	1.78	1.81	1.82	1.82	1.82	1.82	1.82	1.82	1.82	1.82	1.80	1.79	1.80	1.78	1.77	1.78	1.77	1.75	1.74	1.73	1	1	!	ł	;	;	2.28	2.32	2.37	2.37	2.38	2.38	7 37
	403	2.25	2.00	1.92	1.89	1.86	1.74	1.61	1.65	1.66	1.69	1.68	1.67	1.66	1.66	1.66	1.66	1.65	1.65	1.64	1.64	1.63	1.63	1.62	1.61	1.62	1.60	;	ł	-	;	1	ł	2.10	2.14	2.18	2.18	2.18	2.17	2.06
	408	2.59	2.31	2.22	2.18	2.15	2.02	0.0	1.14	1.41	1.61	1.69	1.71	1.73	1.74	1.75	1.73	1.73	1.72	1.71	1.71	1.70	1.70	1.70	1.69	1.68	1.67	1.66	1	!	:	;	1	2.28	2.33	2.39	2.39	2.39	2.38	2 36
į	407	2.06	1.83	1.75	1.72	1.70	1.59	0.65	0.85	1.10	1.24	1.31	1.34	1.35	1.36	1.37	1.36	1.36	1.36	1.36	1.35	1.34	1.34	1.34	1.33	1.32	1.31	1	1	1	1	;	1	1.81	1.85	1.90	1.89	1.89	1.88	1.87
	406	2.26	1.95	1.87	1.84	1.81	1.67	0.58	0.85	1.10	1.25	1,33	1.37	1.38	1.39	1.39	1.39	1.39	1.38	1.38	1.38	1.37	1.37	1.37	1.36	1.35	1.33	1.31	;	1	;	1	1	1.95	2.00	2.06	2.06	2.06	2.05	2.03
	411	2.48	2.19	2.10	2.06	2.03	1.91	-0.25	-0.27	-0.18	0.03	0.25	0.53	0.73	0.90	1.01	1.06	1.11	1.14	1.15	1.16	1.18	1.19	1.20	1.20	1.20	1.19	1.17	1	!	;	1	}	1.83	1.88	1.93	1.92	1.92	1.90	1.89
Nimbor	410	2.77	2.50	2.44	2.41	2.37	2.26	0.41	0.39	0.49	0.68	0.86	1.10	1.30	1.41	1.50	1.54	1.58	1.60	1.62	1.63	1.64	1.65	1.66	1.66	1.67	1.66	1.65	!	1	1	!	1	2.22	2.26	2.31	2.30	2.30	2,28	2.26
R	409	2.27	2.05	1.98	1.95	1.92	1.82	0.23	0.21	0.29	0.44	0.62	0.00	1.08	1.15	1.23	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.34	1.33	1.33	1.32	1.29	;	;	}	1	}	1.80	1.84	1.88	1.87	1.86	1.85	1.83
	414	2.73	2.67	2,51	2.48	2.47	2.39	0.35	0.36	0.38	0.42	0.48	0.57	0.68	0.95	1.14	1.22	1.33	1.41	1.47	1.49	1.53	1.56	1.58	1.60	1.61	1.62	1.58	1.74	1.82	1.86	1.92	1.96	1.99	2.02	2.05	2.04	2.03	2.01	2.00
	413	2.96	2.74	2.68	2.66	2.62	2.52	-0.05	-0.04	-0.02	0.01	0.10	0.25	0.45	0.65	0.86	1.02	1.16	1.28	1.36	1.43	1.46	1.52	1.54	1.57	1.59	1.58	1.56	1.71	1.81	1.89	1.94	1.98	2.05	2.08	2.10	2.08	2.07	2.06	2.04
	412	2.89	2.63	2.58	2.52	2.50	2.40	-0.87	-0.88	-0.87	-0.78	-0.65	-0.50	-0.20	0.00	0.22	0.36	0.54	0.75	0.84	0.91	0.97	1.01	1.05	1.09	1.12	1.13	1.13	1	;	1	1	1	1.73	1.77	1.82	1.81	1.80	1.78	1.77
	417	2.36	2.17	2.13	2.10	2.08	2.06	-0.66	-0.67	-0.63	-0.56	-0.50	-0.40	-0.31	-0.18	0.02	0.24	0.38	0.51	0.61	0.78	0.75	0.81	0.84	0.87	06.0	0.92	0.91	1.03	1.09	1.14	1.19	1.24	1.29	1.29	1.32	1.31	1.31	1.30	1.28
	416	2.73	2.52	2.47	2.46	2.43	2.32	-0.65	-0.66	-0.64	-0.62	-0.56	-0.43	-0.27	-0.12	0.08	0.32	97.0	0.57	0.72	0.78	0.83	0.88	0.97	1.03	1.06	1.08	1.09	1.23	1.31	1.37	1.43	1.47	1.51	1.51	1.54	1.53	1.52	1.51	1.50
	415	3.28	3.04	2.98	2.96	2.93	2.86	-0.95	-0.93	-0.88	-0.84	-0.72	-0.65	-0.48	-0.27	0.0	0.22	0.43	0.62	0.75	0.87	96.0	1.04	1.12	1.17	1.20	1.24	1.26	1.43	1.52	1.61	1.67	1.74	1.78	1.83	1.88	1.86	1.85	1.82	1.80
ocat fone	Elevation	0.56	_										-					•									>	0.57	0.61	0.65	69.0	0.74	0.78	0.81	0.83	0.86	0.88	0.88	0.88	0.88
Discomptor Locations	Station	15.00U	8.79U	6.75U	4.79U	2.790	1.790	0.080	0.22D	0.36D	0.500	0.640	0.780	0.920	1.06D	1.20D	1.34D	1.48D	1.62D	1.76D	1.90D	2.04D	2.18D	2.45D	2.73D	3.010	3.29D	3.710	4.13D	4.55D	4.97D	5.390	5.81D	060°9	6.37D	6.65D	8.02D	9.57D	11.120	12.670
10	No.	4	2	9	7	œ	6	14	15	16	17	18	19	70	21	22	23	57	25	76	27	28	59	30	31	32	33	35	38	7 7	77	47	20	51	52	53	24	55	99	23

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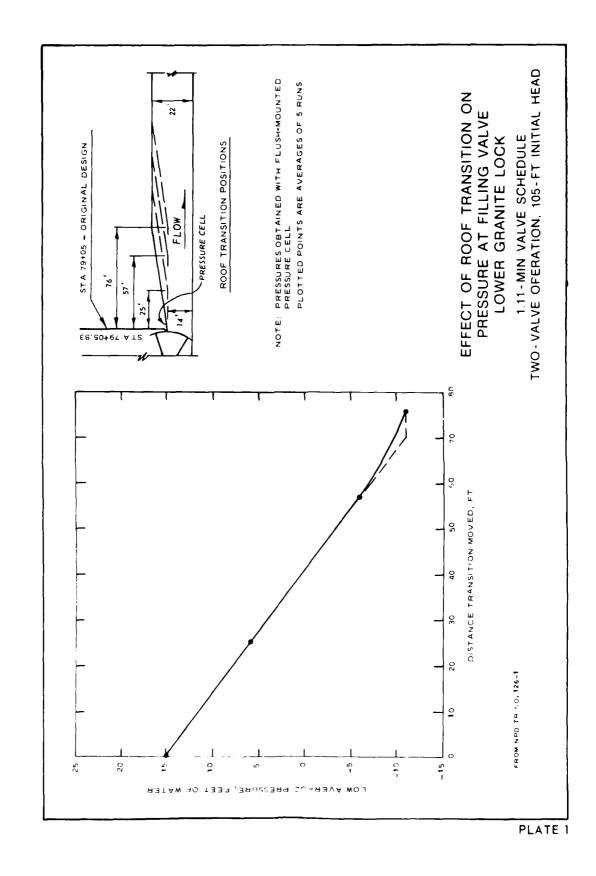
Table 9 Average Piezometer Readings, Type 8 Expansion

		7.00				_																																						
	445	3.61	3,43	3,39	3,36	3.31	3.30	-0.85	-0.84	-0,85	-0.83	-0.79	-0.73	-0.65	-0.52	-0.29	-0.16	3.0	0.21	0.36	87.0 0	٠. اب	0.67	0.88	0.94	90.	1.12	1.17	1.25	1.43	1.35	1.39	1.42	1.44	£ ,	1.51	1.33	1.50		30.1	1.67	44.	0u. t	
	444	2.94	2.78	2.75	2.72	2.70	2.65	-0.78	-0.77	-0.78	-0.77	-0.75	-0.66	-0.59	87.0-	-0.31	-0.17	-0.03	0.10	0.16	0.31	7	0.51	65.0	00.0	28.0	5.0	75.0	96.0	1.02	1.05	1.09	1.13	1.13	<1.1	1.18	٠. د د د	1.5	1.0	0		1.5	٥٠. ١	
	443	2.36	2.25	2.20	2.19	2.17	2.13	-0.57	-0.58	-0.58	-0.57	-0.55	-0.51	-0.48	-0.42	-0.34	-0.18	-0.05	70.0	0.17	0 0	0.38	;;;	0.51	18.0	90.0	0.73	0.76	0.77	08.0	0.83	0.87	68.0	. 6	200	0.60	* o	200	1.02	00.7	6.1	1 05	0	
	44.2	4.29	4.11	60.4	4.07	70.7	3.99	-0.74	-0.75	-0.74	-0.72	-0.69	-0.63	-0.58	-0.47	-0.32	-0.23	00.0	6.17	0.33	0.50	0.01	0.83	0.00	5	1,05	1.21	1.25	1.30	1.35	1.51	1.50	4.	1.39	1.00	0.4	1.1	1 1	1.17) 	1.80	0	ot.	
Sherr #	441	4.03	3.88	3.84	3.83	3.88	3.77	-0.43	-0.45	-0.43	-0.42	-0.40	-0.32	-0.29	-0.19	-0.05	0.04	0.18	0.30	0.39	9:30	97.0	0.0	1.06	27.1	1.16	1.28	1.34	1.39	1.46	1.51	1.56	9c.1	1.63	0 4	: -	4.5		- - -	7		50.	0	
S and	077	2.98	2.88	2.85	2.83	2.81	2.78	-0.42	-0.46	-0.42	07.0-	-0.38	-0.36	-0.34	-0.29	-0.19	-0.14	-0.03	0.13	0.23	0.32	; ;	75.0	05.0	0.71	0.81	0.89	0.92	0.95	1.01	1.06	01.10	1.12	1.14	111	01.1	1.20	1.22	1.23	1.25	1.27	1.26	1.25	
	439	2.56	2.51	2.49	2.47	2.45	2.42	-0.02	0.00	-0.02	0.03	0.05	0.07	0.10	0.17	0.25	0.32	0.41	0.45	0.00	65.0	00.00	6.0	98.0	0.88	0.94	1.02	1.04	1.07	1.11	1.14	1.16	1.19	1.21	1 25	1 27	1.29	1.31	1.33	1.35	1,33	1.32	1.3	
	438																																											
-	437	3, 32	3.26	3.24	3.22	3.21	3.19	-0.35	-0.37	-0.35	-0.33	-0.32	-0.29	-0.26	-0.22	-0.13	80.0	-0.02	70.0	0.17	0.19	35.0	0.41	0.53	0.64	0.73	0.77	0.81	0.83	0.86	0.89	0.94	6.6	1.03	1.05	1.07	1.09	1.10	1.11	1.12	1.12	1.11	1.10	
	436																																											
	34 435		4.13 4.8		4.81			0.51 0.28			0.52 0.31																					1.49 1.55												
	433 4	-1	3.13 4.					0.30								0.37					0.57 0.					0.83 1.						1.03		•		_	_	_	1.12 1.	_	_		_	
ations	Elevation	0.56		_			_										_		_			-	0.57									0.09					0.78	0.81	0.83	0.86	0.88	0.88	0.88	
Piezometer Locations	Station	15.000	36.78	36./3	76/.r	1 791	1.190	0.090	0.220	0.360	0.00	0.00	0.780	1.045	1 200	3,40	7.530	1.620	1.760	1 900	2.040	2.18D	2.32D	2.46D	2.60D	2.740	2.880	3.020	3.160	3.300	2,440	3.720	3.860	4.000	4.140	4.28D	4.42D	4.700	4.98D	5.26D	8.020	9.580	11.140	
Pfe	3	.,	<u>.</u>	c r	~ ?	6 9		1 1	<u>:</u>	<u>.</u>	2 2	0 9	5	2, 7	1.0	; ~	3 ~	. ×	2.4		. 82	56	30	31	35	33	<u> </u>	£ ;	£ ;	٠,	2 0	Ç 07	7	42	6.4	7,7	45	94	1.4	87	5,4	55	9,6	

* Refer to Table 1 for flow conditions for each run.

Table 9 (Concluded)

Pi	Piezometer Locations	cations							i	Run Numb	-1.5						:
S.	Station	Elevation	877	677	463	462	461	451	452	453	454	455	456	457	454	654	6.9
4	15.00U	0.56	2.64	3.29	3.14	2.52	2.24	1.88		3,55		1,59	2.45	3.24	2.22	- S	1.87
5	3.790	_	2.47	3.11	2.91	2.37	2.11	1.73		3.33		1.44	2.34	2.98	1.91	87.7	56
9	6.750		2.43	3.05	2.89	2.33	2.08	1.70		3.26		1.41	2.30	2.92	1.86	2.25	14.
7	4.79U		2,42	3.03	2.85	2.31	2.06	1.68		3.23		1.38	2.27	2.88	1.82	2.16	3.7
œ	2.790		2.39	3.01	2.82	2.28	2.04	1.67		3.20		1.37	2.25	2.86	1.80	2.14	0+
6	1.790		2.36	2.95	2.73	2.22	1.98	1.63		3.11		1.30	2.16	2.76	1.72	2.03	2.27
17	0.080	-	-0.38	-1.10	-1.33	-0.75	-0.41	-0.44		-0.24		-0.46	-0.58	-0.60	0.35	0.25	0.35
15	0.22D	_	05.0-	-1.12	-1.41	-0.85	-0.57	-0.45		-0.23		-0.45	-0.57	-0.55	0.32	6.23	0.28
16	0.36D		-0.38	-1.10	-1.44	-0.93	-0.59	-0.44		-0.26		-0.43	-0.55	-0.50	0.36	0.3%	0.4]
17	0.500		-0.34	-1.12	-1.43	-0.97	-0.57	-0.43		-0.22		-0.38	-0.53	-0.41	65.0	0.65	9.0
18	0.64D		-0.32	-1.08	-1.36	-0.87	-0.55	-0.3′		-0.18		-0.32	-0.40	-0:30	0.76	0.85	0.93
19	0.780	_	-0.24	-1.02	-1.30	-0.81	-0.48	-0.29		-0.0-		-0.22	-0.24	-0.11	0.91	1.67	1.16
20	0.920		-0.19	-0.88	-1.26	-0.75	-0.42	-0.20		0.16		-0.08	-0.04	0.18	1.06	1.23	1.43
71	1.06D	-	-0.05	-0.74	-1.11	-0.62	-0.33	-0.07		67.0		0.03	0.10	0.05	1.16	1.32	51
22	1.200		0.03	-0.40	~0.83	· · · 0-	-0.14	0.10		0.60		0.18	07.0	0.65	1.21	1.47	1.5
23	1.340		٥.13	-0.25	-0.64	-0.36	-0.03	0.17		0.74		0.26	0.51	0.82	1.23	1.4.	1.63
57	1.48D	_	0.25	00.00	-0.42	-0.17	0.11	0.30		1.01		0.37	0.67	1.02	1.25	7	1.66
25	1.620		0.38	0.21	-0.16	00.0	0.21	0.41		1.17		27.0	e.∵e	1.16	1.27	1.46	1.65
56	1.76D	_	0.54	0.34	0.03	0.15	0.34	87.0		1.27		97.0	0.87	1:3:	1.29	1.48	1.70
27	1.90D		0.62	97.0	0.19	0.25	0.43	0.55		1.38		67.0	0.92	1.28	1.28	3.48	1.71
28	2.04D		0.69	0.67	0.28	0.37	65.0	0.58		1.43		0.52	0.97	1.33	1.27	1.46	1.70
53	2.18D	-	0.75	0.72	0.47	0.45	0.56	0.61		1.46		0.53	0.98	1.36	1.24	· ;	1.65
30	2.32D	0.57	0.84	0.78	0.56	0.54	0.62	0.64		1.54		0.56	1.03	1.42	1.27	1.46	1.69
31	2.46D	0.58	0.92	0.88	0.61	0.63	0.68	0.68		1.61		0.61	1.11	1.50	1.34	4.55	1.80
35	2.60D	0.60	0.95	0.93	0.70	0.67	0.72	0.71		1.66		0.64	1.16	1.56	1.39	1.60	1.85
33	2.74D	0.61	1.02	1.02	0.81	0.73	0.75	0.76		1.72		0.67	1.20	1.62	1.4.	1.65	1.91
34	2.880	0.62	1.07	1.11	0.86	0.77	0.79	0.80		1.78		71	16	1.67	1.45	1.70	1.94
: ::	3.020	0.64	1.10	1.17	0.91	0.79	0.83	0.83		1.81		0.72	1.28	1.7;	1.48	1.73	1.97
٤ ;	3.160	0.65	1.12	1.20	0.94	0.84	0.86	0.86		1.85		0.75	1.33	1.78	1.51	1.78	7.0
÷ ?	3.300	0.67	1.15	1.24	0.97	0.88 0.08	0.89	0.88		16.1		0.78	1.34	1.80	1.53	1.80	2.05
ž č	3.440	0,08	1.17	1.30	1.01	0.93	0.93	0.40		1.94		08.0		1.85	1.56	Z .	7.30
607	3 7 20	0.69	1.20	1.36	1.03	0.96	0.93	26.0		 		79.0	1.51) (i) (i)	y	<u> </u>	7.7
7	3.860	0.72	1.28	1.38	1.08	10.01	000	76.0		50.7		78	;		7	,	
77	4.000	0,74	1.31	1.40	1.11	1.03	1.02	0.96		2.09		0.86	1 1	5	. 4	· · ·	0000
7 3	4.14D	0.75	1.33	1.42	1.16	1.04	1.04	0.98		2.11		0.87	1.50	3	1.67	5	
77	4.280	0.76	1.35	1.44	1.19	1.05	1.06	1.00		2.14		0.89	1.53	2.03		00.7	53.5
45	4.421	0.78	1.38	1.46	1.23	1.07	1.08	1.02		2.17		0.41	1.56	5.0	1.71	·0·.	55
4,7	4.70D	0,81	1.40	1.51	1.26	1.11	1.10	1.03		5.19		0.93	1.60	2.16	1.7.	10.1	5.3
47	4.980	0.83	1.42	1.54	1.30	1.14	1.13	1.05		2.22		96.0	1.6%	5.13	1.77	2.14	7
00 ·	5.26D	0.86	1.43	1.58	1.34	1.17	1.15	1.07		2.18		86.0	74.	77.	1.80		3
7,	8.020	98.0	1.44	1.61	1.35	1.19	1.14	1.08		2.30		1.16	æ	¥0.7	٥,٠١	41.	
<u>.</u>	9.580	0.88	1.43	1.60	1.34	. 18	1.13	1.08		?:		1.30		7.05	1: 7	3.	; ;
9	11.140	0.88	1.42	1.39	1.33	1.17	1.12	1.07		5.30		1.12	1.8	5	1.73	<i>?</i> :	9
2.7	17.700	0.88	1.41	1.58	∷.	 	1.1	1.04		2.28		1.15	1.87	80.7	7:38	3 	9



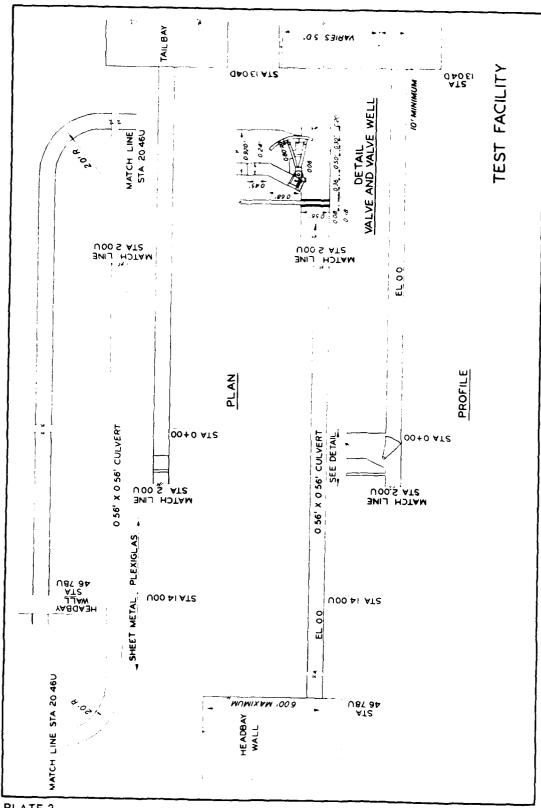
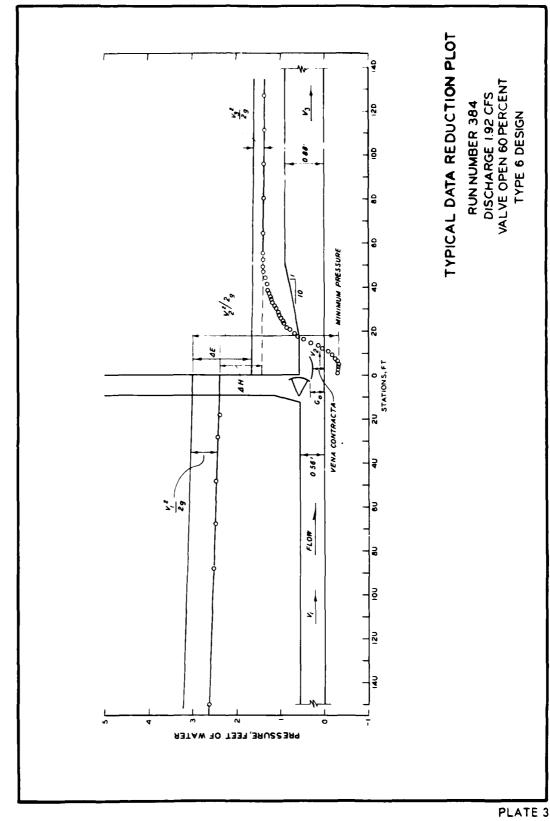


PLATE 2



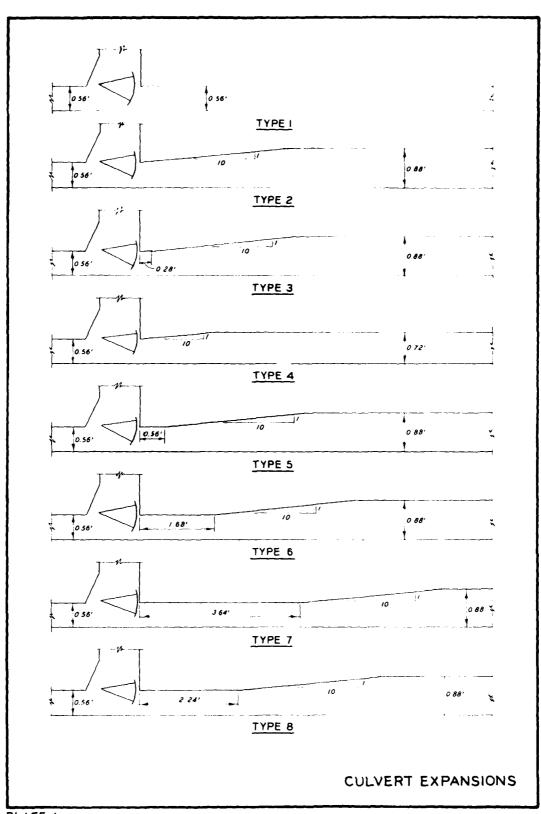


PLATE 4

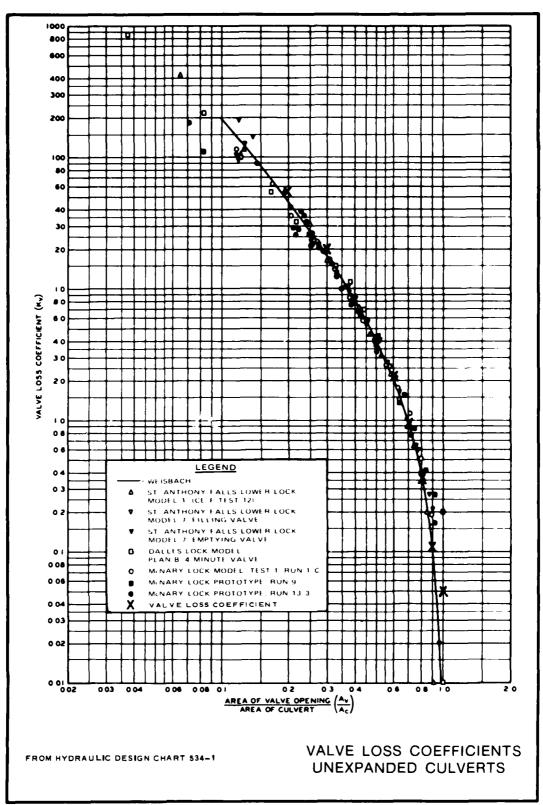


PLATE 5

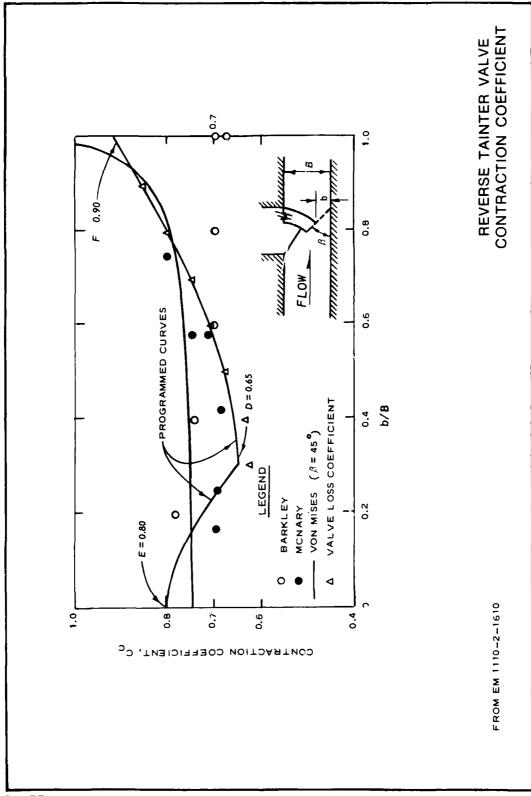


PLATE 6

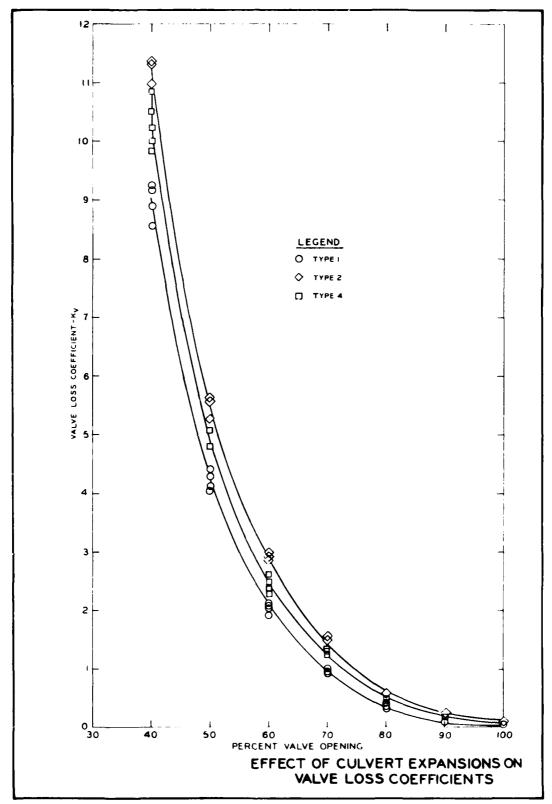


PLATE 7

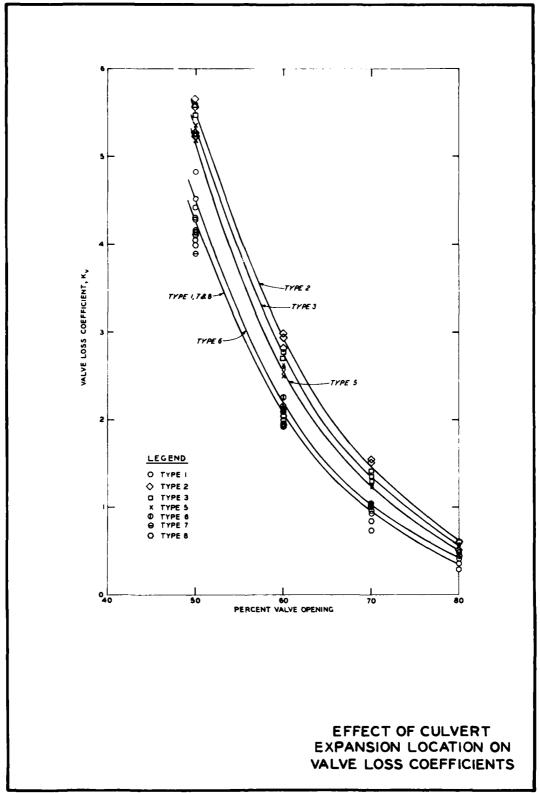


PLATE 8

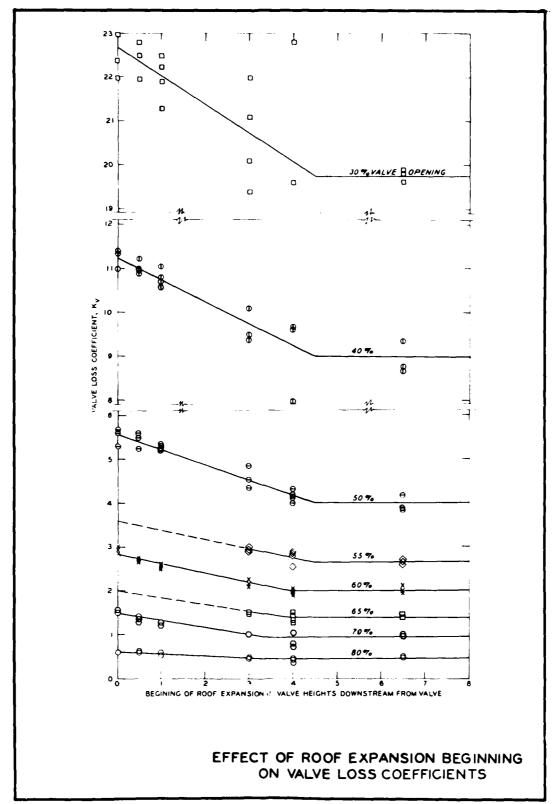


PLATE 9

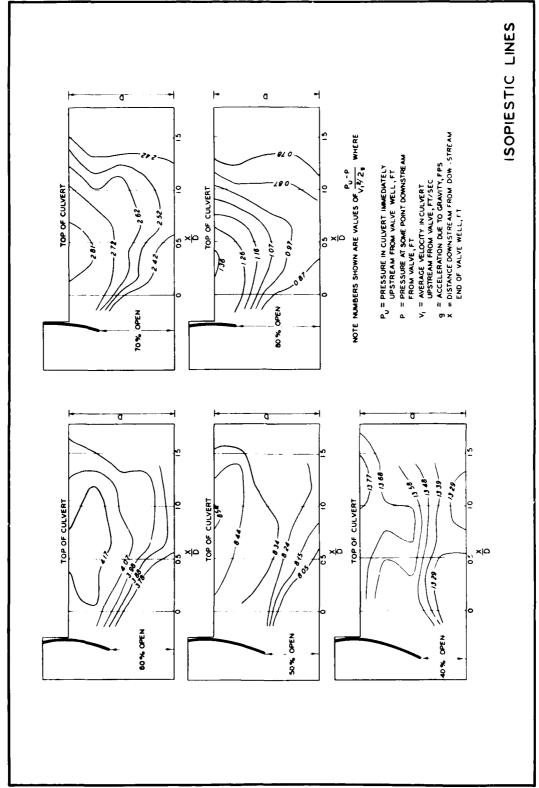


PLATE 10

In accordance with letter from MAEN-RDC, DAEN-ASI dated 22 July 1977, Subject: Facsimile Catalog Cards for Laboratory Technical Publications, a facsimile catalog card in Library of Congress MARC format is reproduced below.

Pickering, Glenn A. Lock culvert valve loss coefficients: hydraulic laboratory investigation / by Henn A. Pickering (Hydraulics Laboratory, U.S. Army Engineer Waterways Experiment Station). -- Vicksburg, Miss. : The Station; Springfield, Va.; available from NTIS, 1981. 15, [21] p., 10 p. of plates : ill. ; 27 cm. -- (Technical report / U.S. Army Engineer Waterways Experiment Station ; HL-81-10) Cover title. "September 1981." Final report. "Prepared for Office, Chief of Engineers, U.S. Army." 1. Culverts. 2. Locks (Hydraulic engineering). 3. Pressure--Measurement. 4. Valves. I. United States. Army. Corps of Engineers. Office of the Chief of Engineers. II. U.S. Army Engineer Waterways Experiment Station. Hydraulics Laboratory. III. Title .V. Series: Technical report (U.S. Army Engineer Waterways Experiment Station); HL-81-10. TA7.W34 no.HL-81-10

